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19XRV Familiarization, Maintenance, Troubleshooting

Chee Nee Bong

October 2012

19XRV



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Overview

19XRV Overview

19XRV Components

Compressor Theory

Maintenance

19XRV

Chiller



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- Semi Hermetic Centrifugal Chiller
- Tonnage
 - 19XR - 200 to 1,500 Nominal Tons (703 to 5275 kW)
 - 19XRV with Variable frequency Drive - 200 to 1,450 Nominal Tons (703 to 5100 kW)
- Chlorine Free HFC-134a Refrigerant
- Semi Hermetic Motor
- ASME Heat Exchangers



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Chiller Identification



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Carrier
A United Technologies Company

MODEL NUMBER 19XRV5050446LCH64-
SERIAL NUMBER 2911Q21017

MACHINE NAMEPLATE SUPPLY DATA

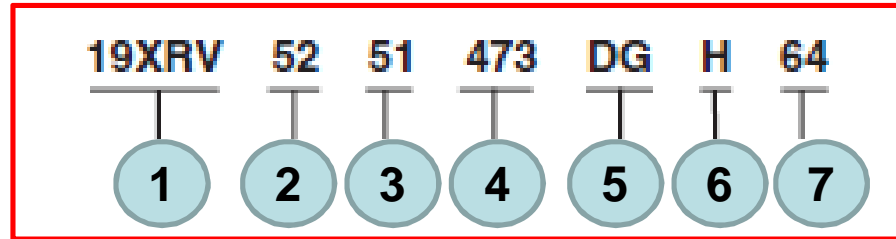
VOLTS/PHASE/HERTZ	460 / 3 / 60
LOCKED ROTOR AMPS	454
OVERLOAD TRIP AMPS	490.32
MAX FUSE/CIRCUIT BREAKER SIZE	1000
MIN SUPPLY CIRCUIT AMPACITY	567

MACHINE ELECTRICAL DATA

MOTOR NAMEPLATE VOLTAGE	460 V
COMPRESSOR 100% SPEED	60
RATED LINE VOLTAGE	460
RATED LINE AMPS	454
RATED LINE KILOWATTS	335
MOTOR RATED LOAD KW	325
MOTOR RATED LOAD AMPS	522
MOTOR NAMEPLATE AMPS	545
MOTOR NAMEPLATE RPM	3567
MOTOR NAMEPLATE KW	387
INVERTER PWM FREQUENCY	4 KHZ

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Chiller Identification



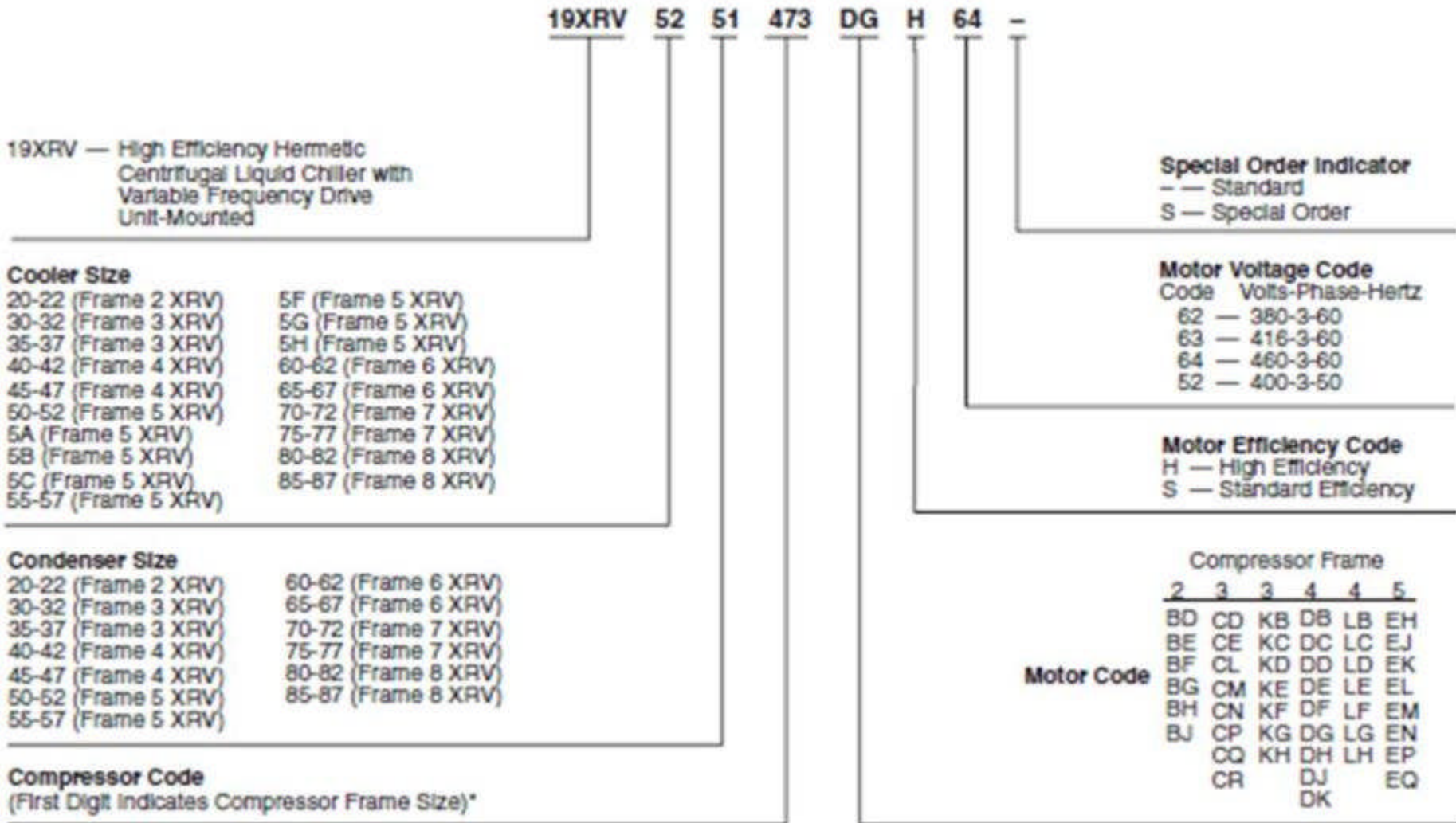
1. Chiller Type (High Efficiency Hermetic Centrifugal Chiller with Variable Frequency Drive Unit-mounted)
2. Cooler Size
3. Condenser Size
4. Compressor Code
5. Motor Code
6. Motor Efficiency Code
7. Motor Voltage Code

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Chiller Identification



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*Second digit will be a letter (example 4G3) on units equipped with split ring diffuser.

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Compressor Code



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19XRV 52 51 473 DG H 64

4

7

3

•Wheel diameter – Lift

•Wheel Shroud Size – Capacity
•Alphabet – Unit with split ring diffuser

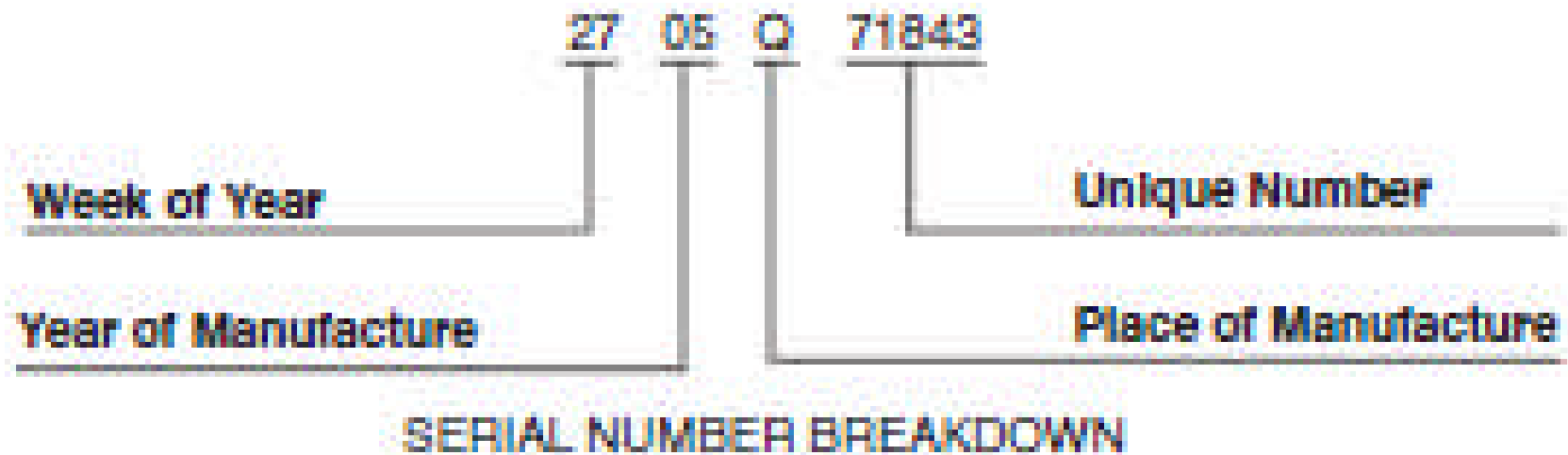
- Compressor Frame Size 2,3,4,5
- Frame 2 – Up to 350 tons
- Frame 3 – Up to 550 tons
- Frame 4 – Up to 900 tons
- Frame 5 – Up to 1600 tons

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Chiller build date and serial



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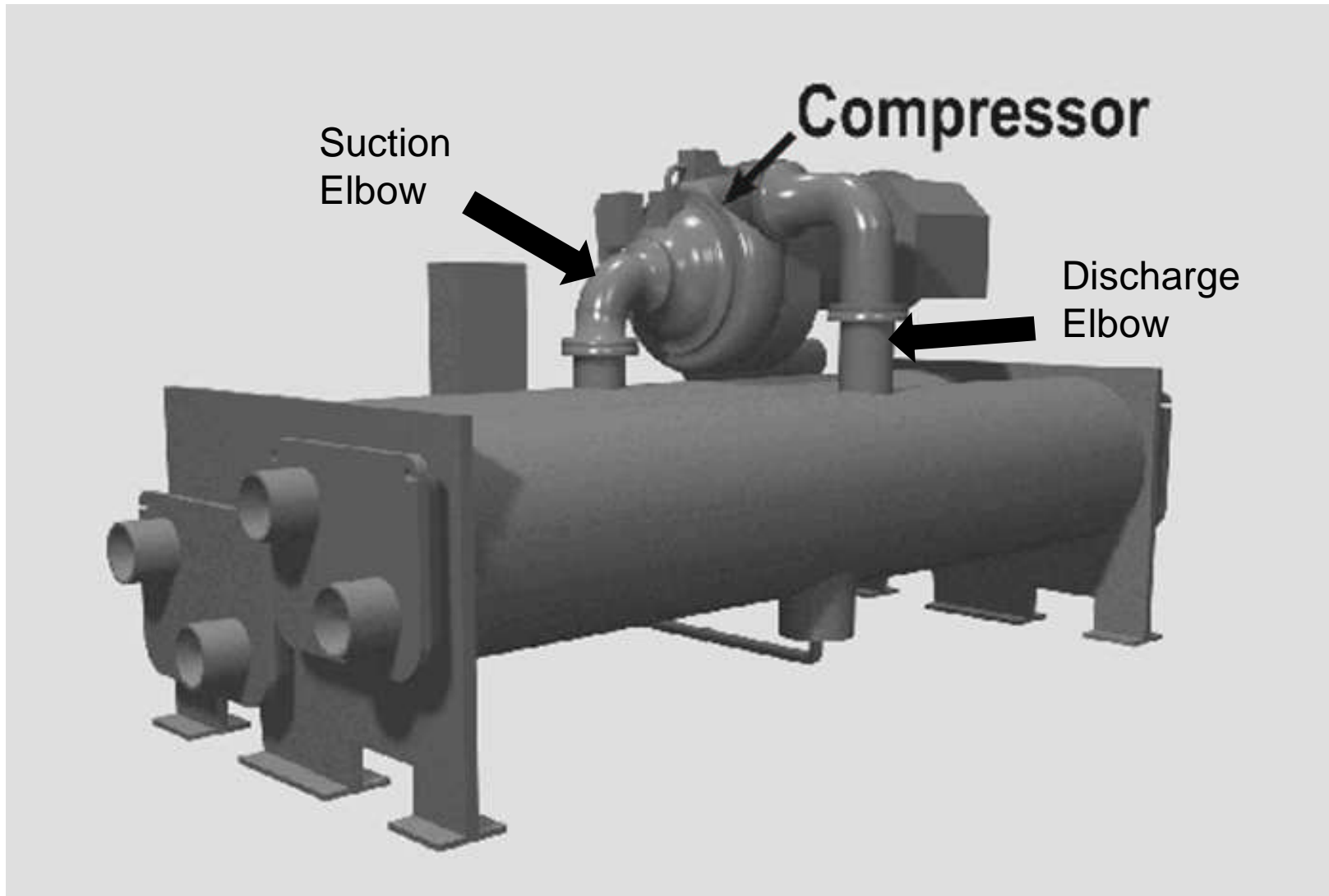


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Chiller



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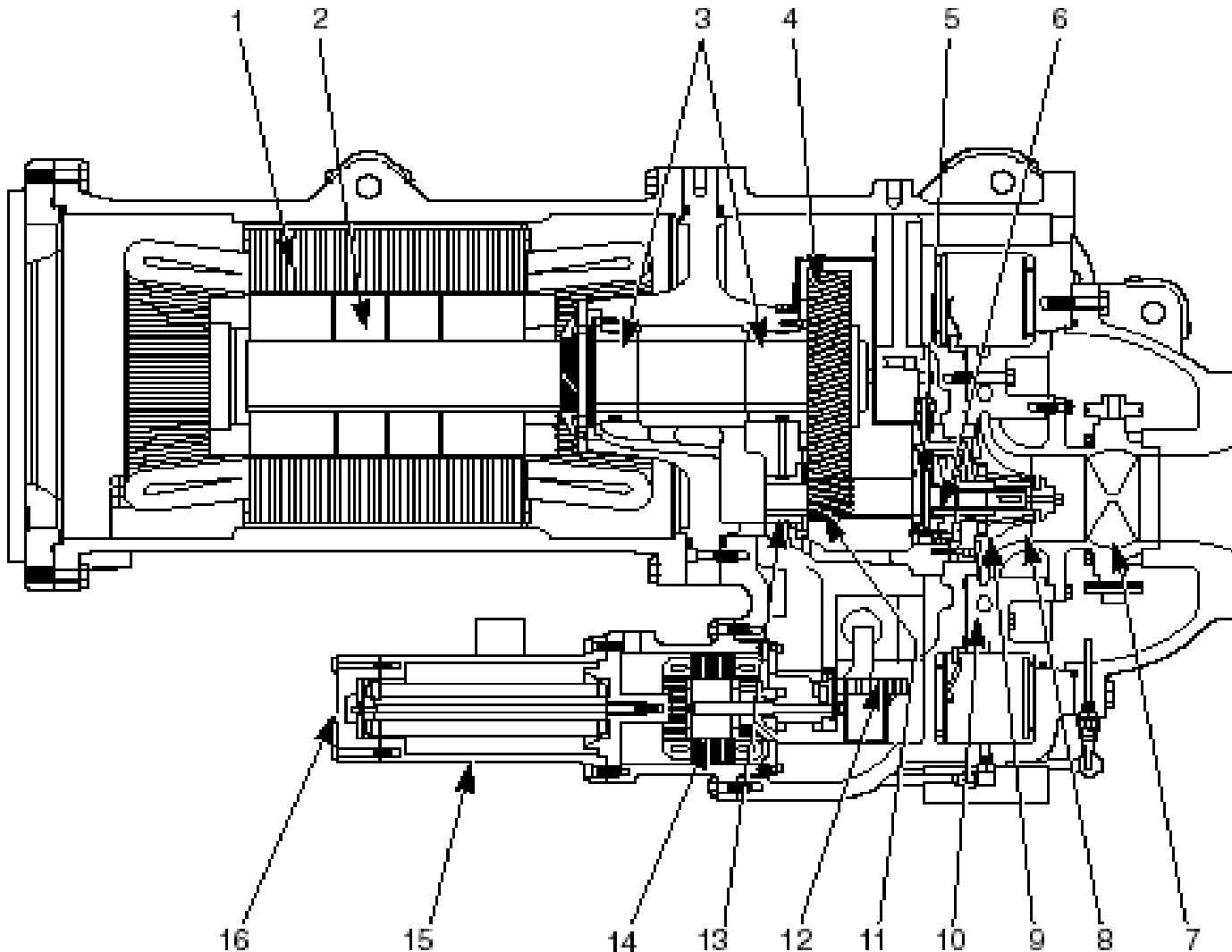
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COMPRESSOR COMPONENTS



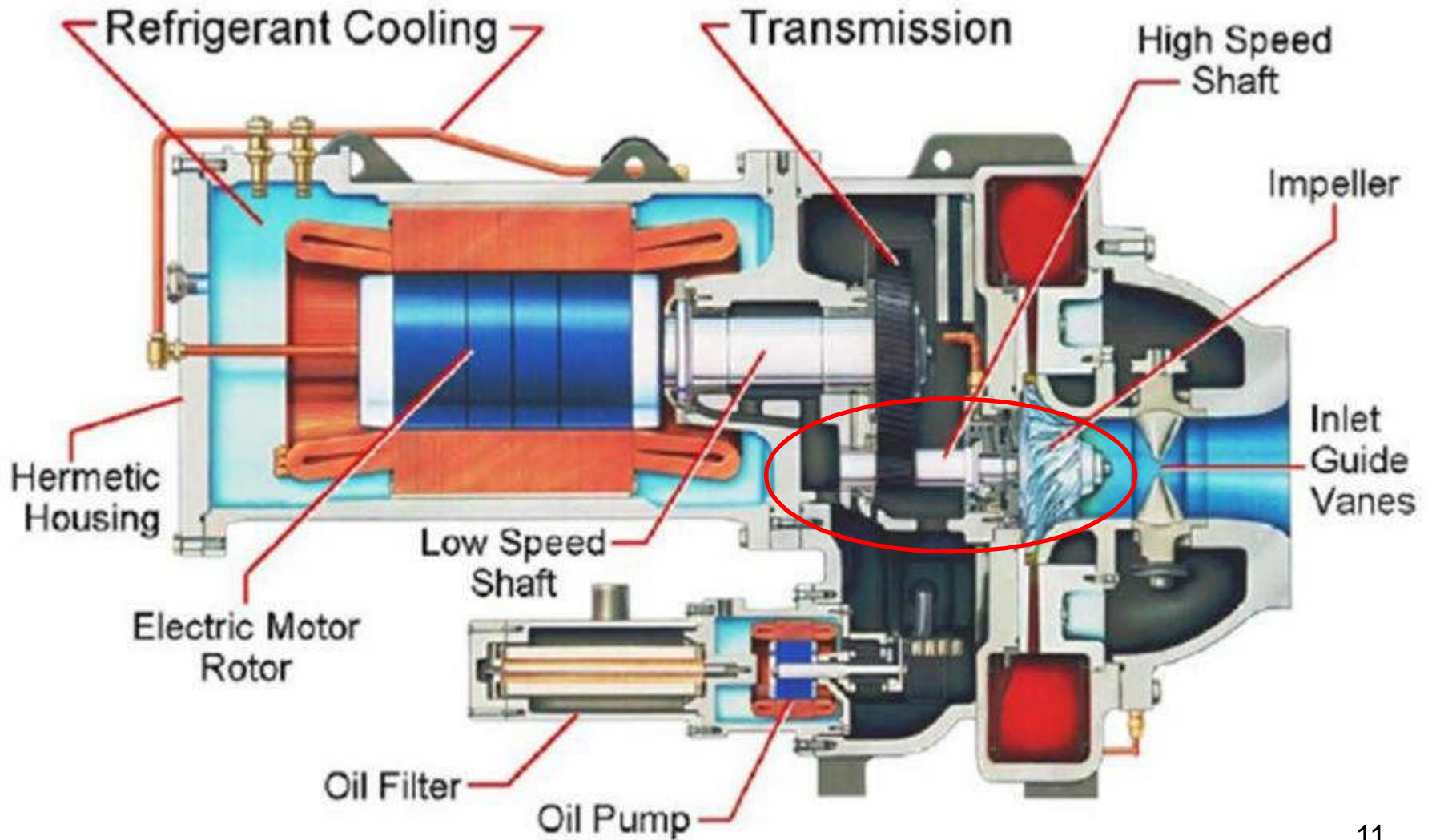
- 1. Motor Stator
- 2. Motor Rotor
- 3. Motor Shaft
- 4. journal bearings
- 5. Low Speed bull gear
- 6. High speed shaft thrust bearing
- 7. High speed shaft bearing
- 8. IGV
- 9. Impeller shroud
- 10. Impeller
- 11. Pipe Diffuser
- 12. High Speed pinion gear
- 13. Oil heater
- 14. High Speed shaft bearing
- 15. Oil pump motor
- 16. Oil Filter
- 17. Oil Filter Cover

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Compressor Section View



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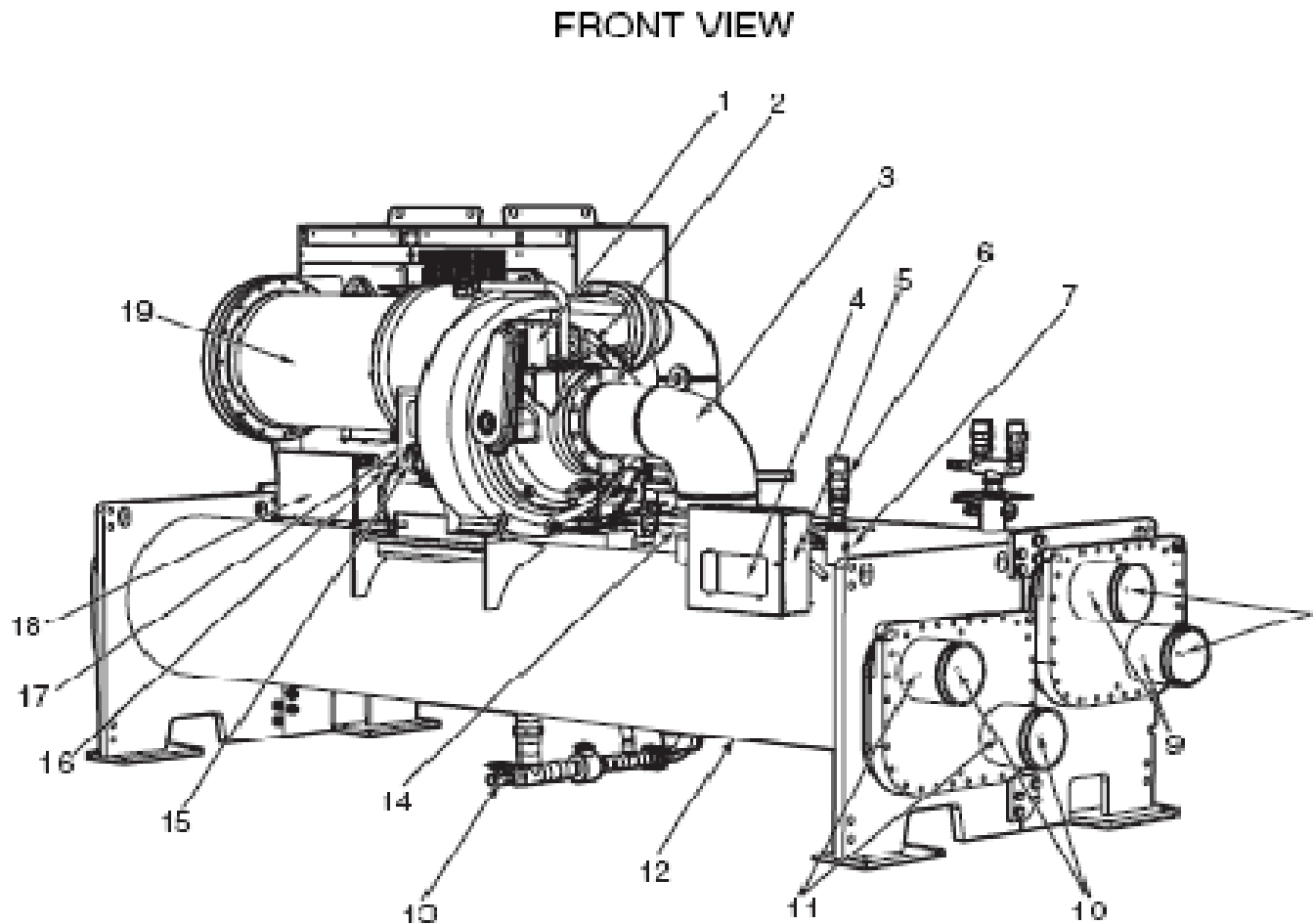


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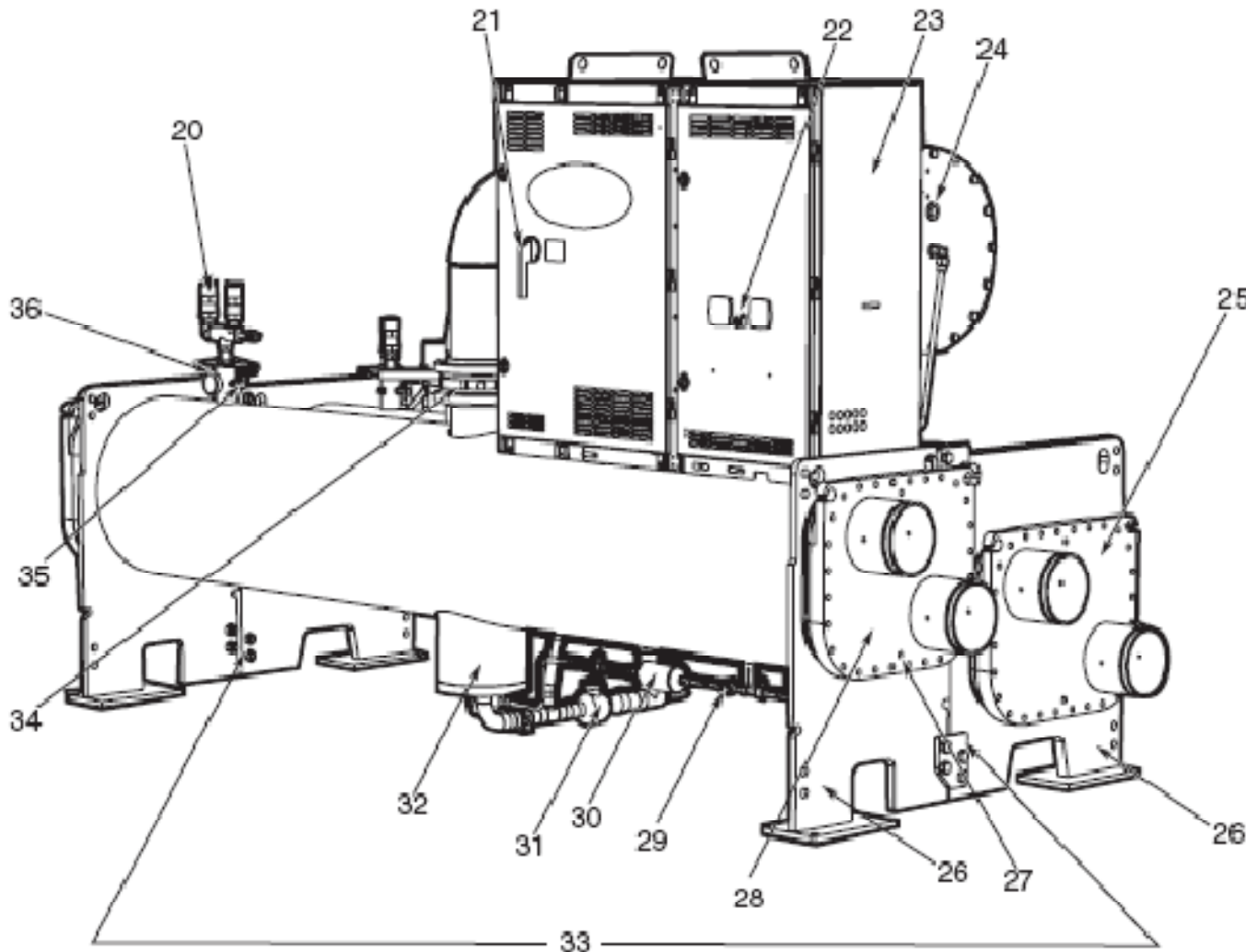
1. Guide vane Actuator
2. SRD Actuator
3. Suction Elbow
4. ICVC
5. Chiller ID Plate
6. Cooler Relief valves
7. Cooler Press Transducer
8. Cond I/O Temp
9. Cond flow device (optional)
10. Cooler Flow device (optional)
11. Cooler I/O Temp
12. Evap Saturation Temp
13. Liquid Line Service Valve
14. Flange connection
15. Oil level SG
16. Oil Cooler
17. Oil drain/charging valve
18. Power Panel
19. Motor housing

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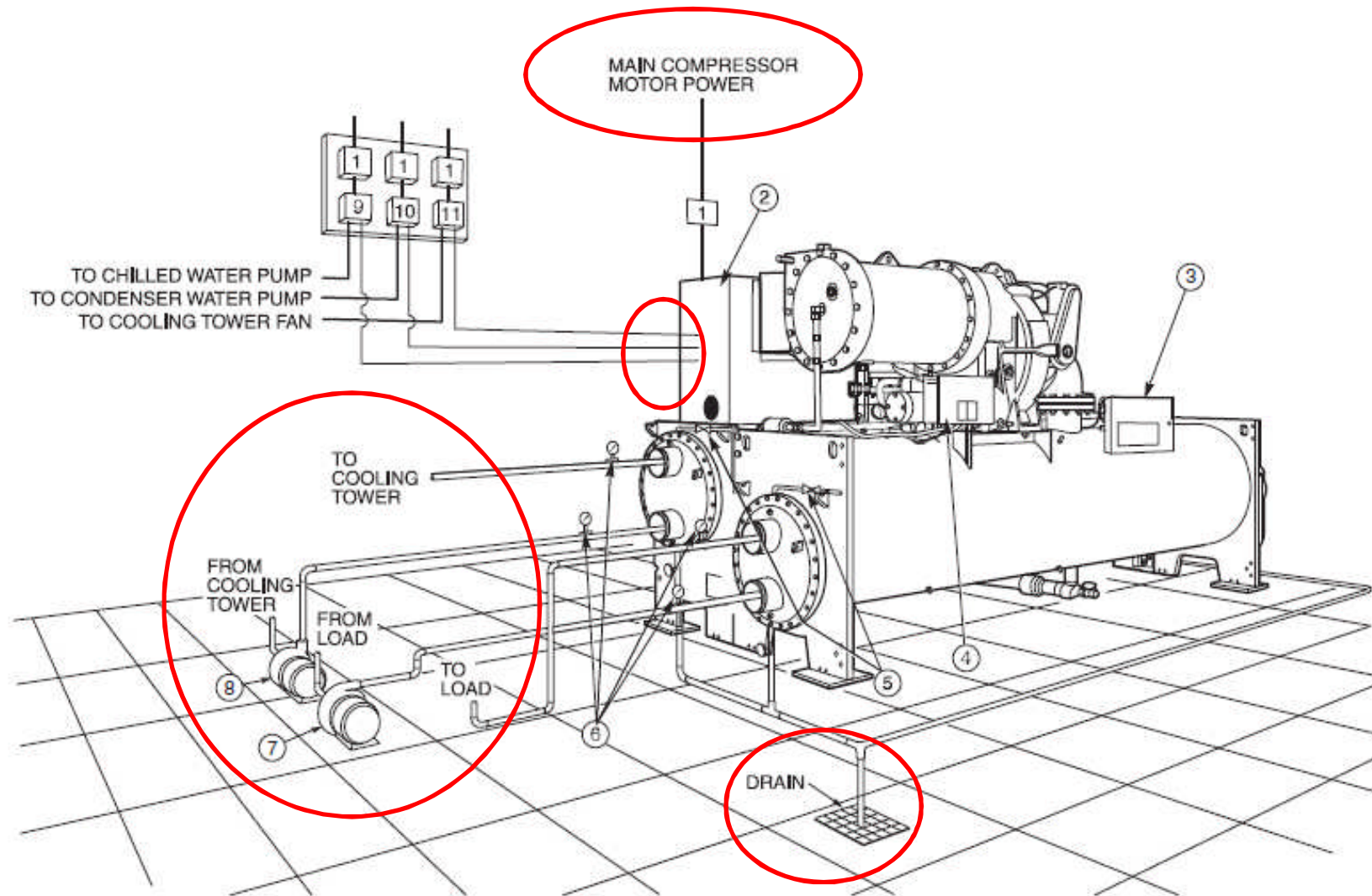
- 20. Condenser relief
- 21. VF circuit Breaker
- 22. VFD Meter Package
- 23. VFD
- 24. Motor Sight glass
- 25. Cooler waterbox Cover
- 26. ASME Nameplate
- 27. Waterbox drain
- 28. Condenser waterbox cover
- 29. Moisture/Flow indicator
- 30. Refrigerant filter/drier
- 31. Liquid line isolation (optional)
- 32. Linear Float valve chamber
- 33. Tubesheet mounting brackets
- 34. Discharge Isolation (optional)
- 35. Refrigerant charging valve
- 36. Condenser pressure transducer

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Field Connections



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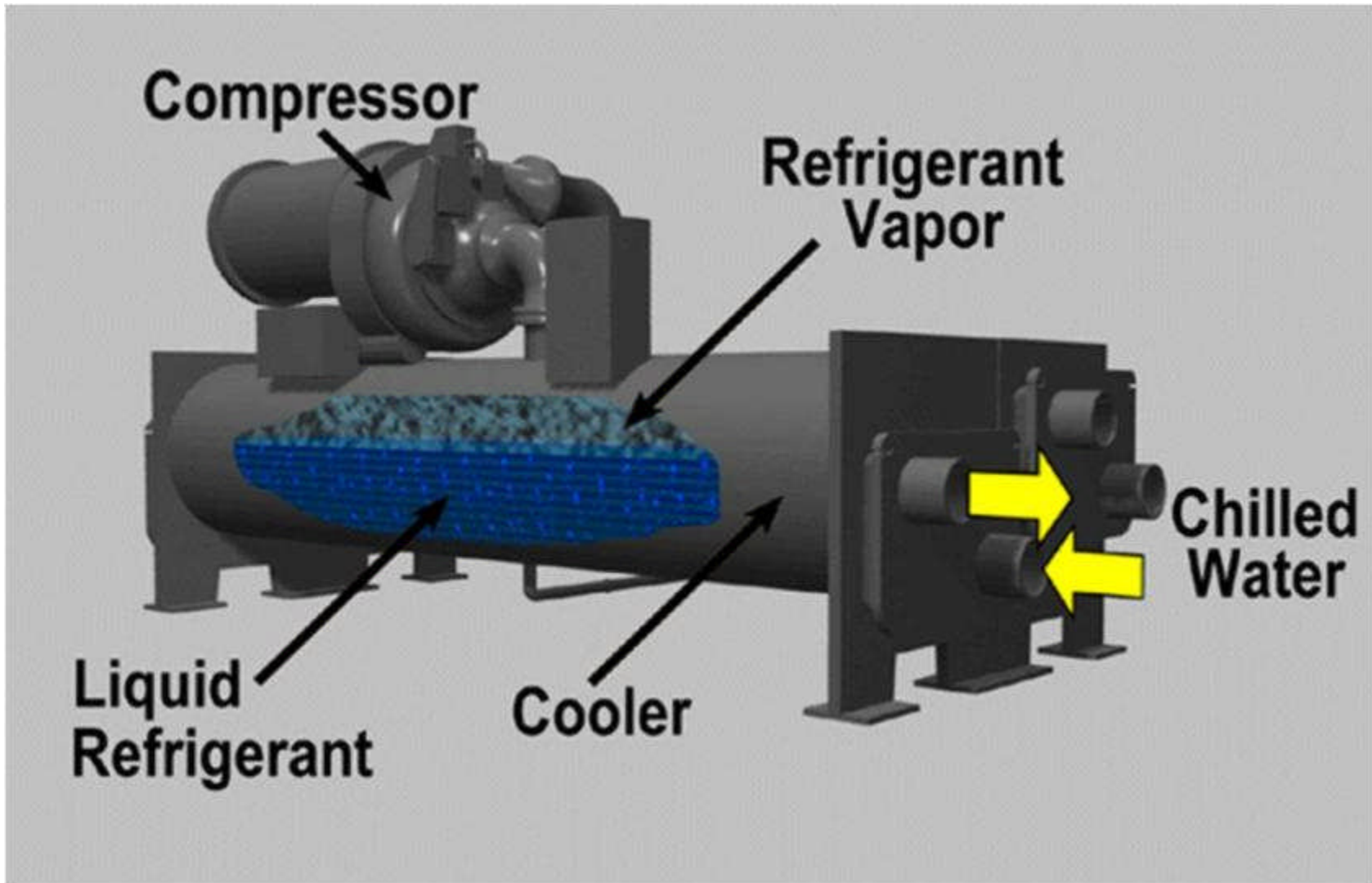


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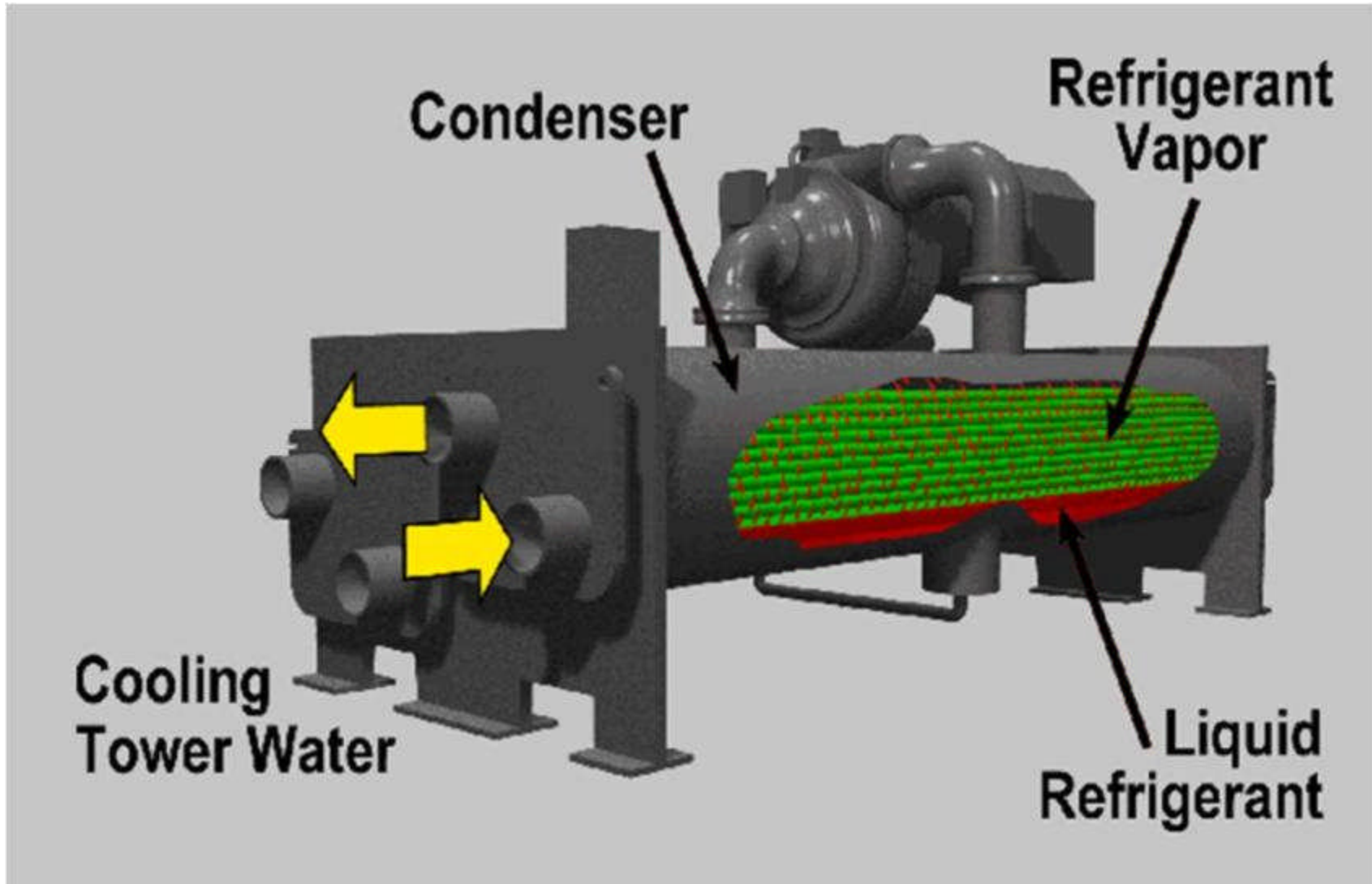


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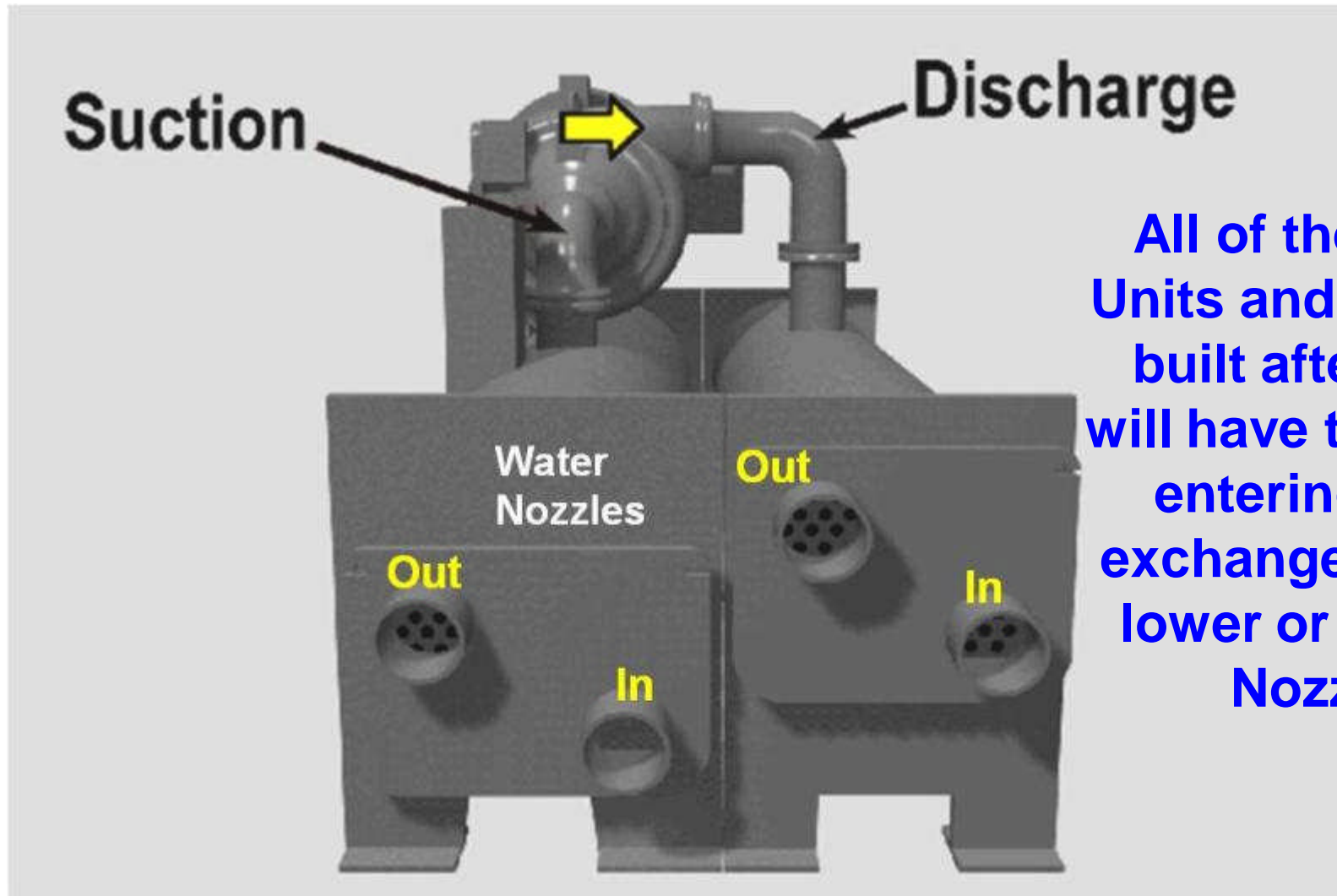


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All of the 19XR Units and any unit built after 1992 will have the water entering heat exchanger on the lower or bottom Nozzle.

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The vessels are a shell and tube design with a relief valve setting of approximately 185psi or 115°F



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Condenser Components are:

- Impingement Baffle
- Flasc Chamber
- Flasc Orifices(2)
- Linear Float
- Tubes with support sheets



Cooler Components are:

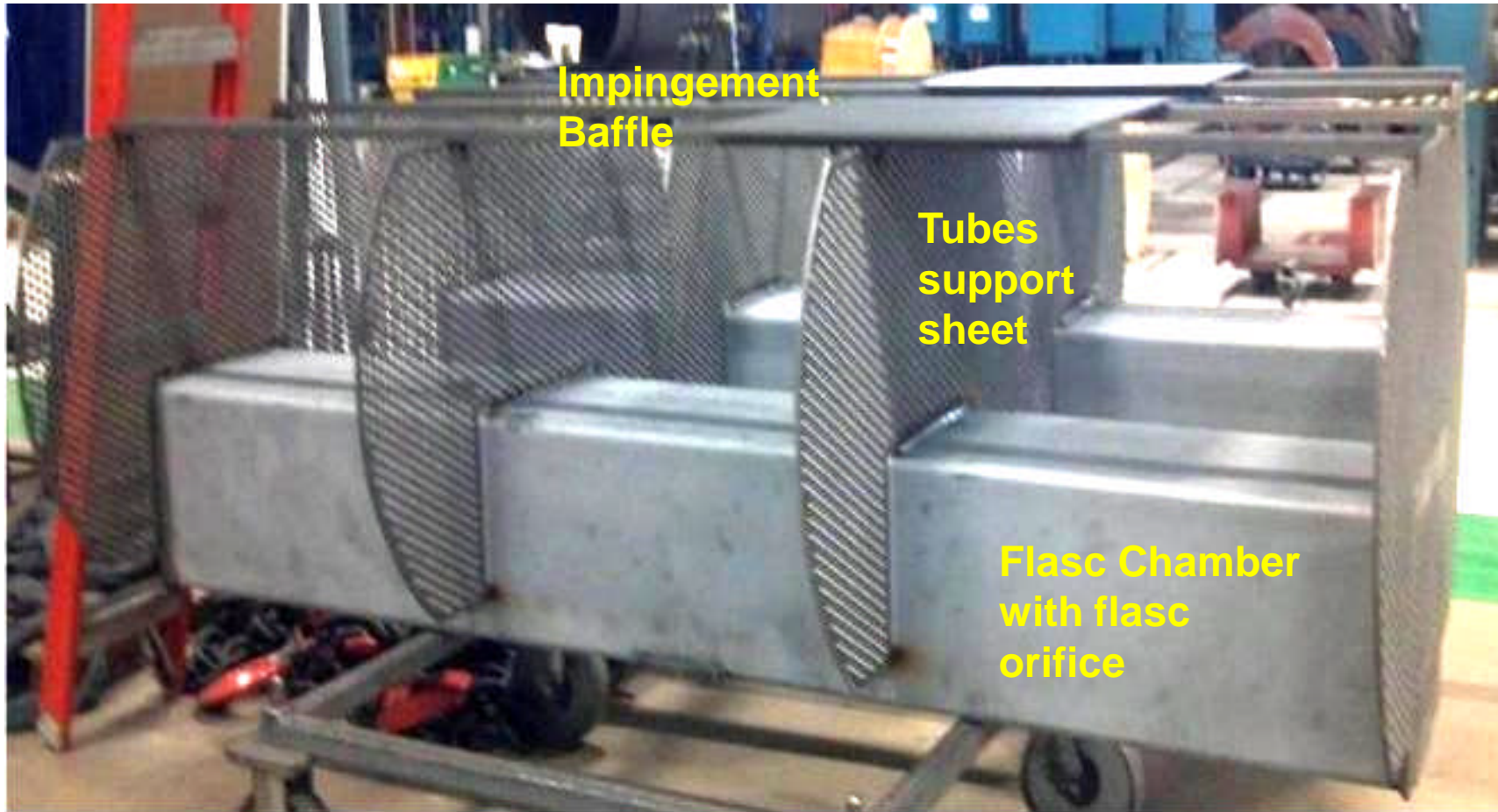
- Distribution chamber
- Tubes with support sheets

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Condenser Flasc Chamber & Tube Sheet



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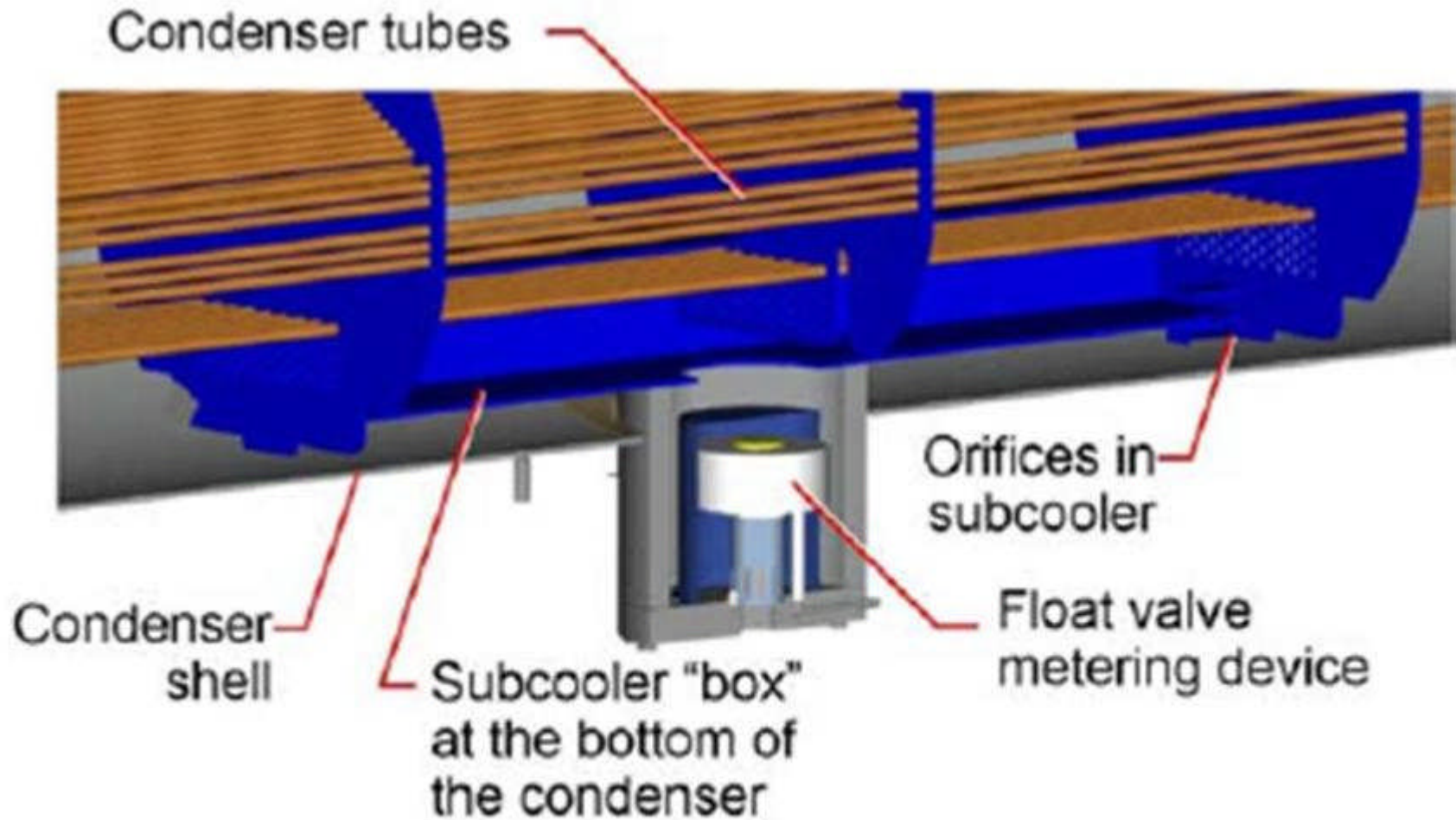


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Condenser Subcooler



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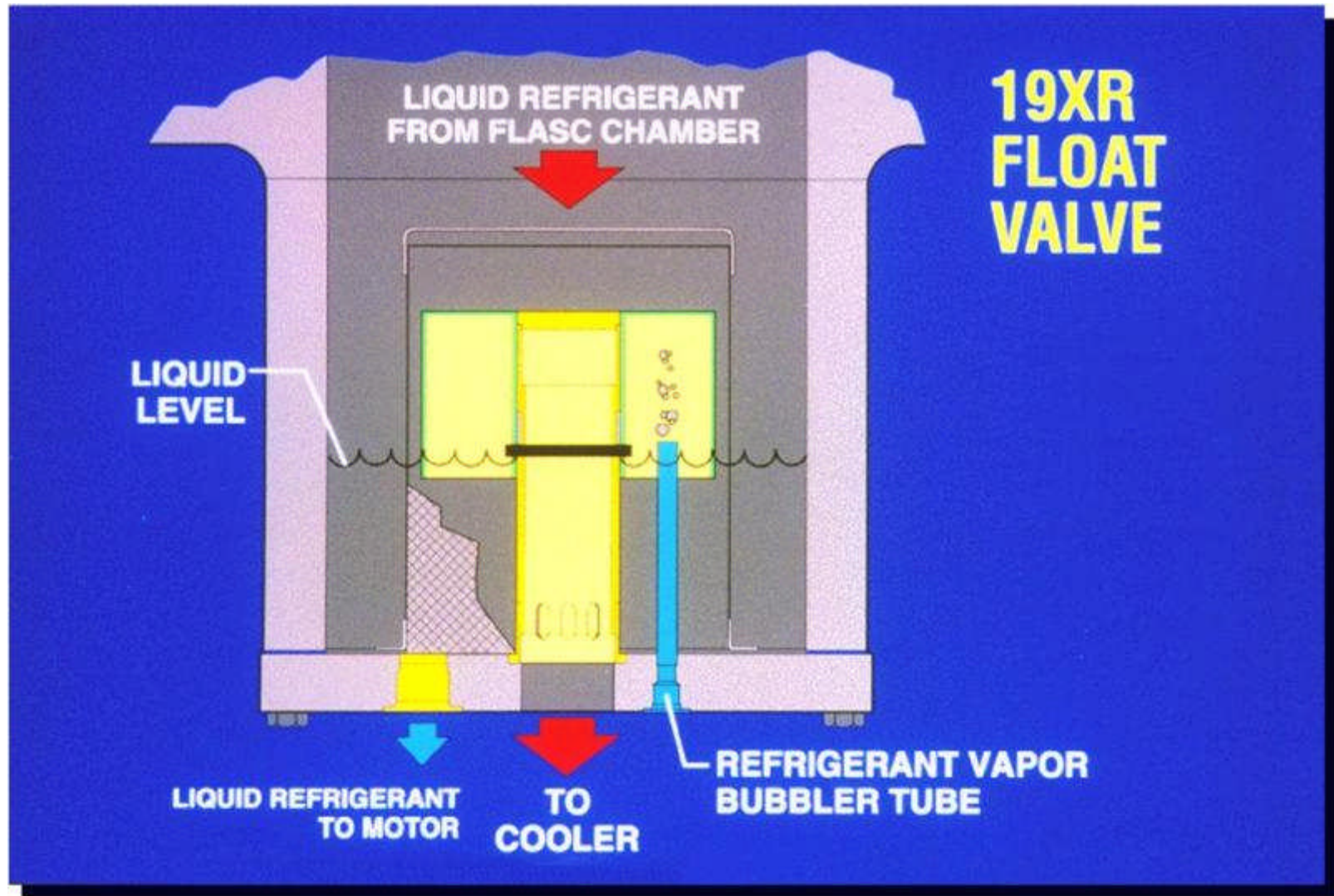


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Float Valve



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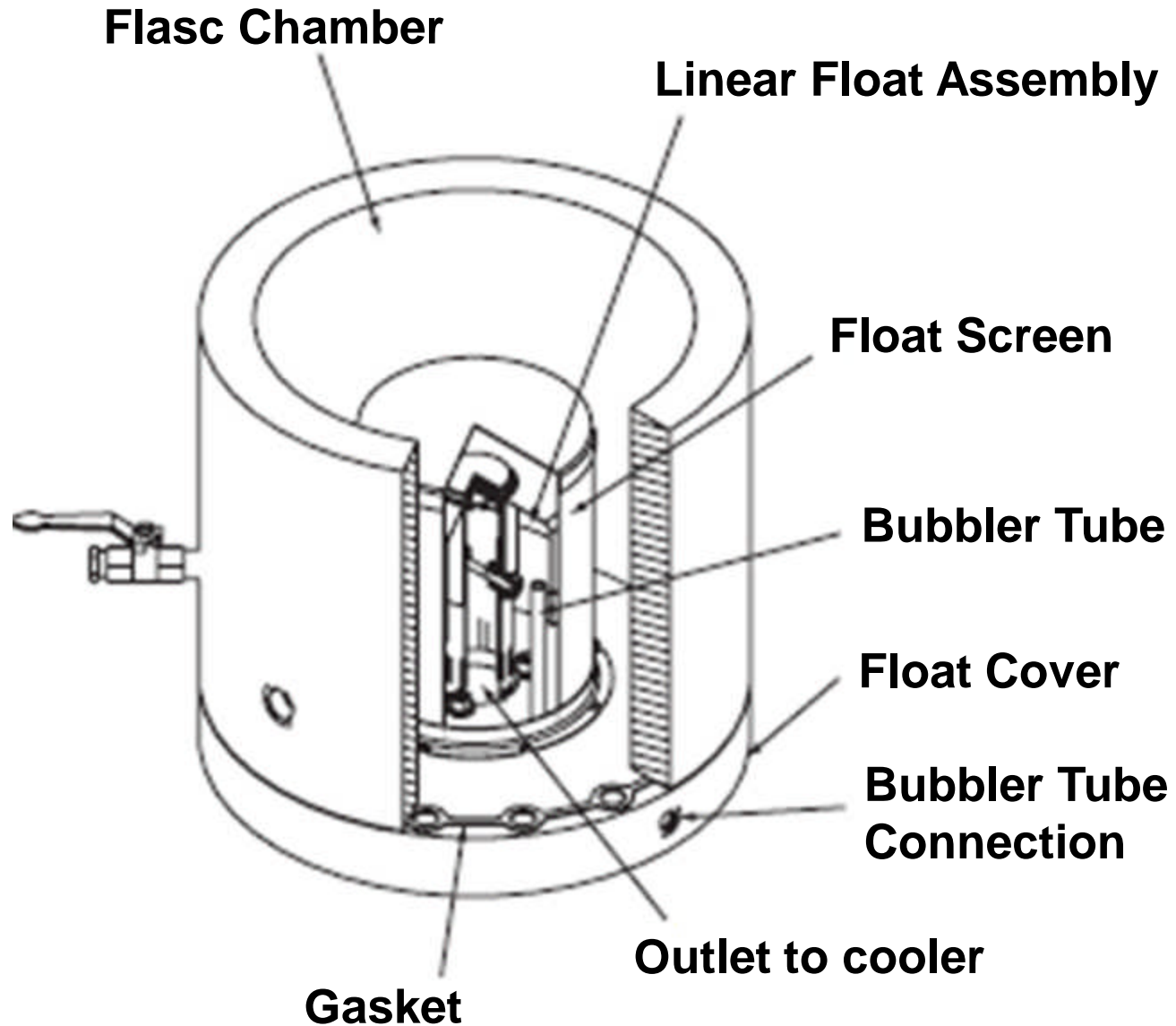


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Float Valve



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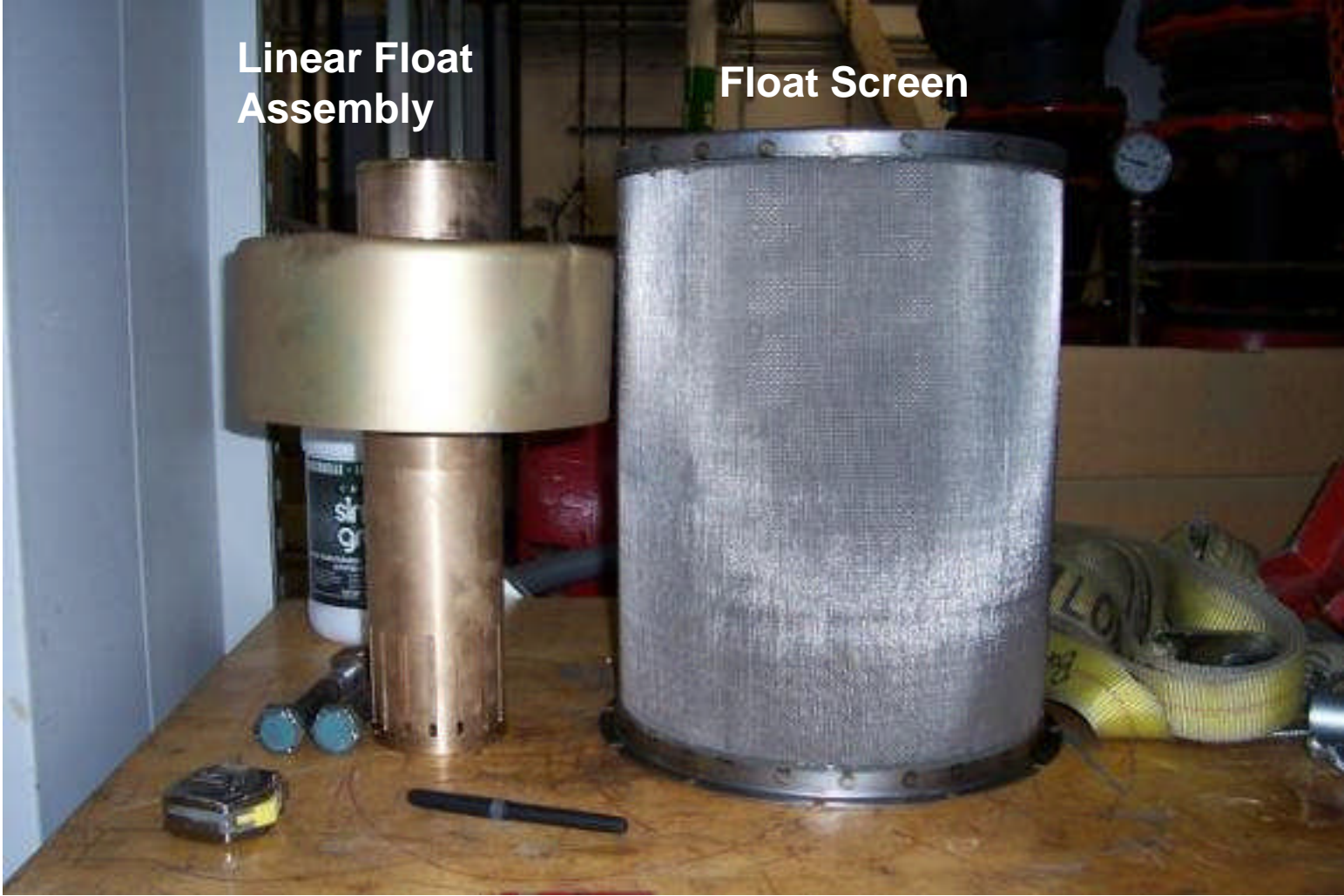


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Float Valve



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Linear Float Assembly

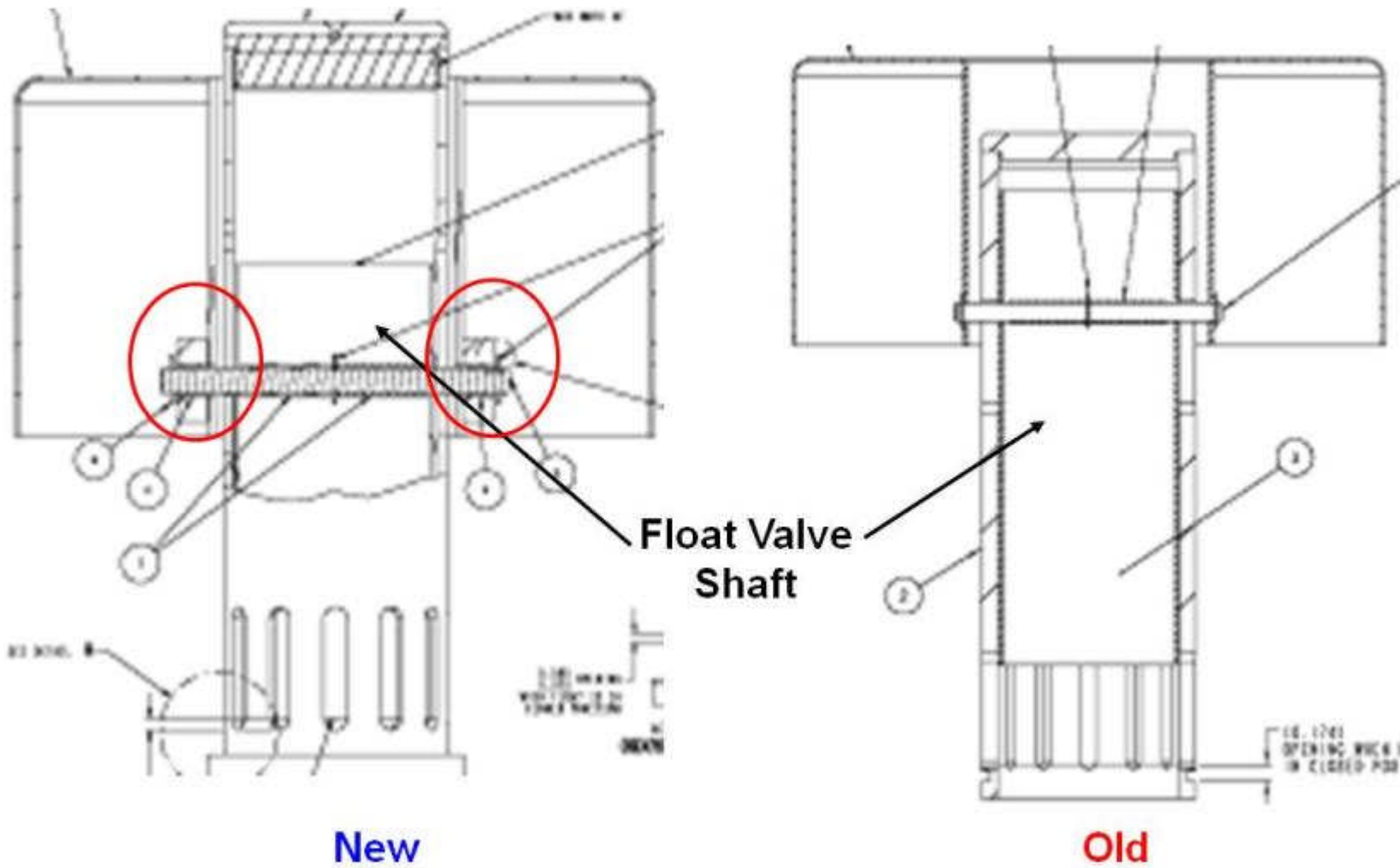
Float Screen

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Float Valve



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Float Valve

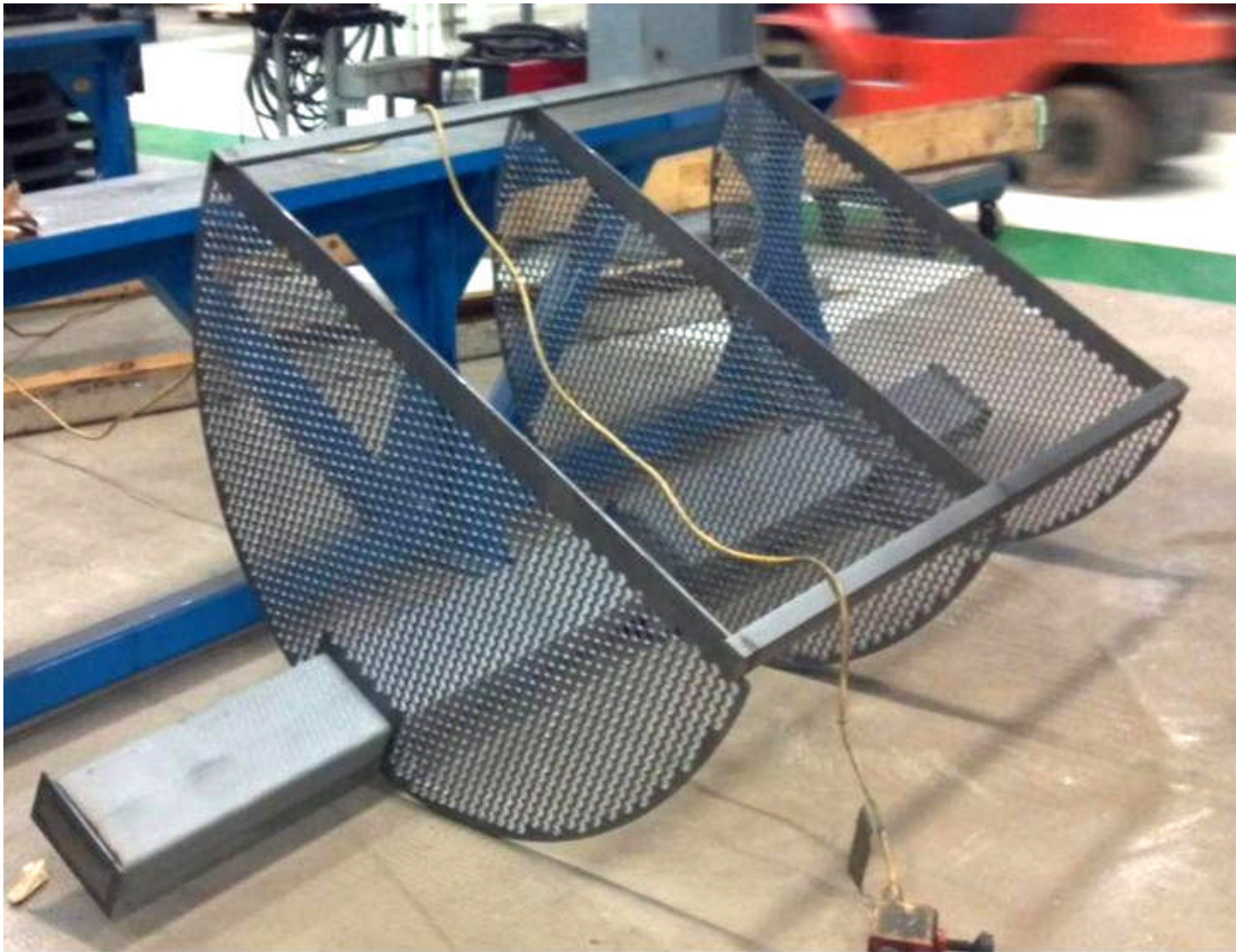


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Evaporator distribution chamber & support sheet



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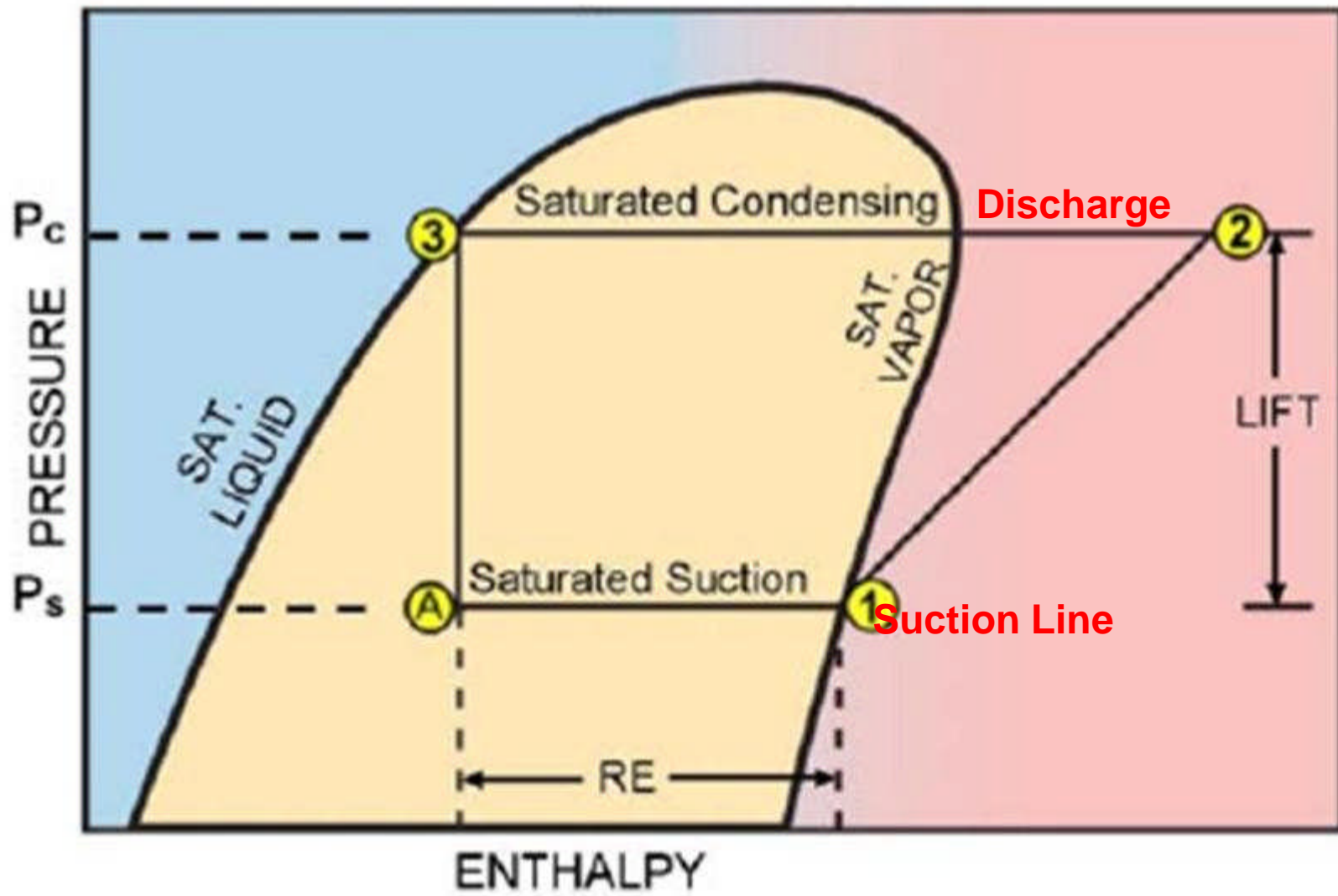


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Chiller



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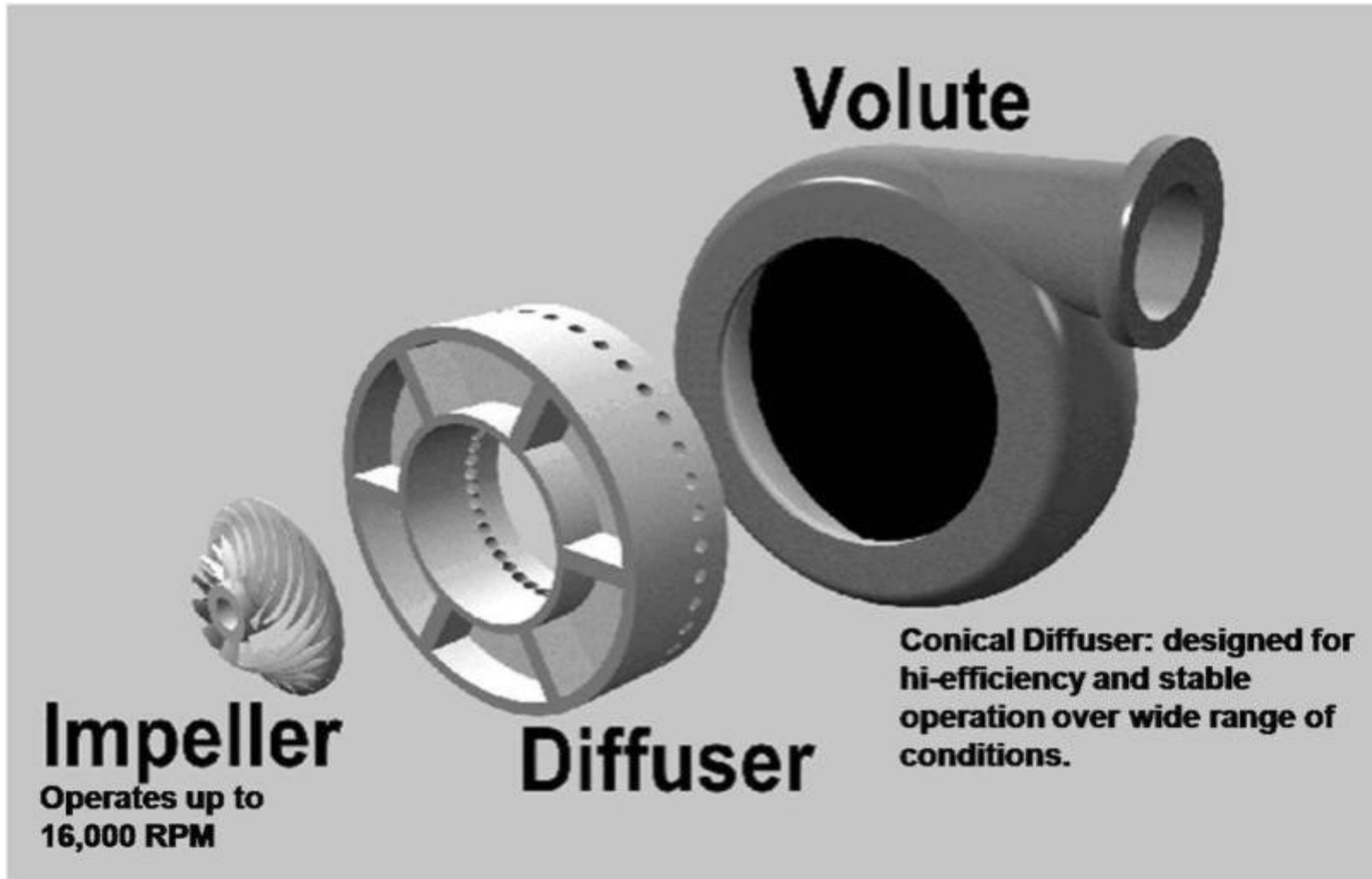


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Compressor Theory



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Compressor Theory

1. Impeller

- Low pressure refrigerant enters the comp through the eye of impeller
- The blade of impeller form flow passages for refrigerant
- Impeller rotates at high speed and as the gas flow towards the tip, momentum increase and that increases the static pressure



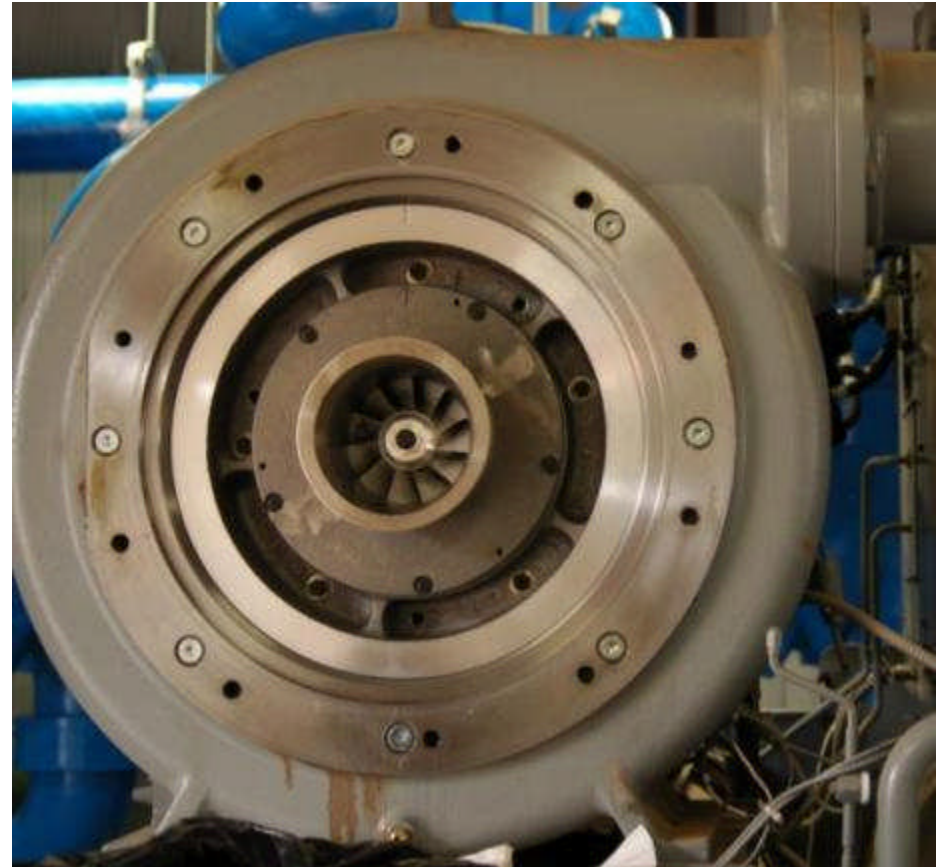
Compressor Theory

1. Diffuser

- From the tip of impeller, refrigerant flow into diffuser.
- Refrigerant is decelerated.
- The dynamic pressure drop, converted to static pressure rise, causing static pressure to increase further

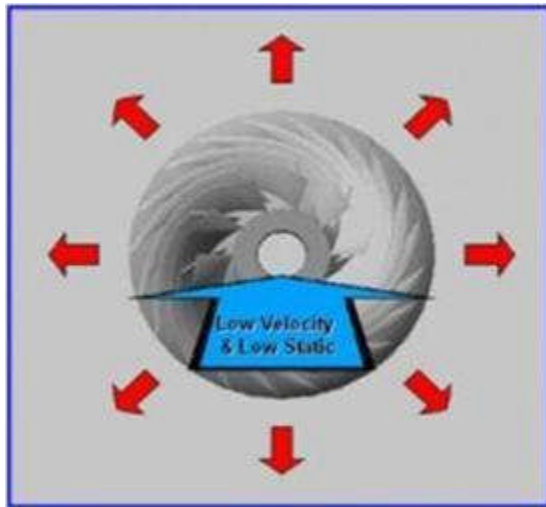
2. Volute

- Vapor from diffuser enters volute, the shape of volute creates more velocity while it directs pressurized refrigerant out of compressor



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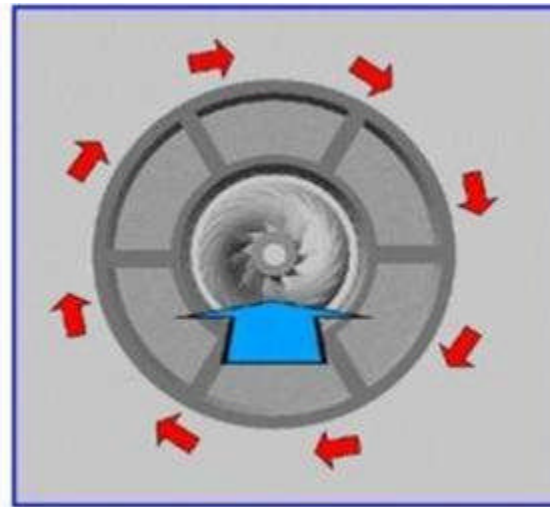
Compressor Theory



The refrigerant follows Bernoulli's Basic "Law of conservation of Energy"

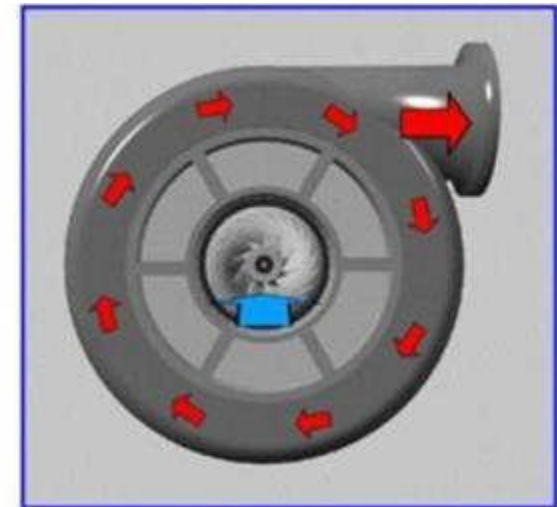
Leaves the Impeller Tips @ High velocity, Low static

Accelerate Refrigerant Vapor



Diffuser pipes slow down the vapor to convert to high static, low velocity.

Changes flow direction



The Volute collects the vapor and conveys it to the discharge connection.

Compressor Theory

Step 1- Refrigerant is drawn into the impeller and accelerates the gas imparting “Kinetic Energy or the energy of motion”

Step 2- The accelerated refrigerant discharges from the compressor flowing through the diffuser passage. The passages increase in size, allowing the gas to expand, reducing the velocity. The kinetic energy is converted to static pressure.

The radial and tangential forces combine to generate the energy to convert the kinetic energy to static pressure

The radial force is directly proportional to the volume or CFM of the refrigerant handled

The tangential velocity is directly proportional to the impeller rotational speed times the impeller diameter

Inlet Guide Vane

What is the purpose of Inlet Guide Vane ?

The inlet guide vanes control the unit capacity by metering the refrigerant vapor flow through the compressor.

The guide vanes are closed at start up reducing the inrush current of the motor at start up.

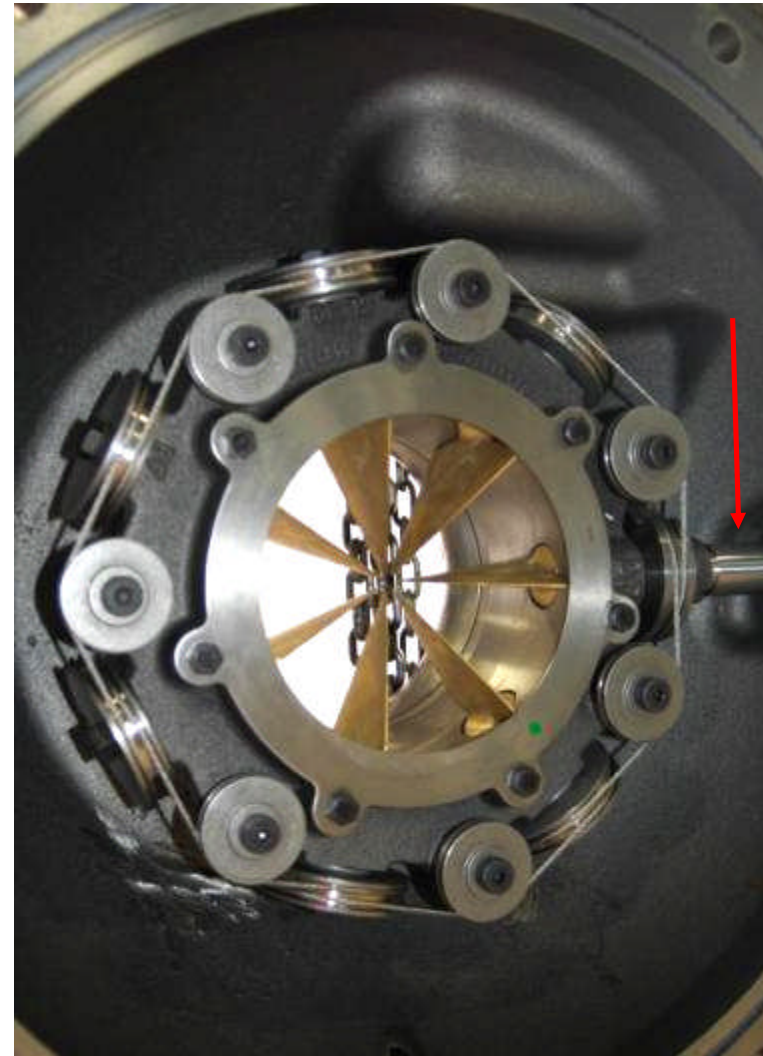
The inlet guide vanes are limited by motor current and Leaving Fluid temperature.

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Compressor Theory – Guide Vane Actuator



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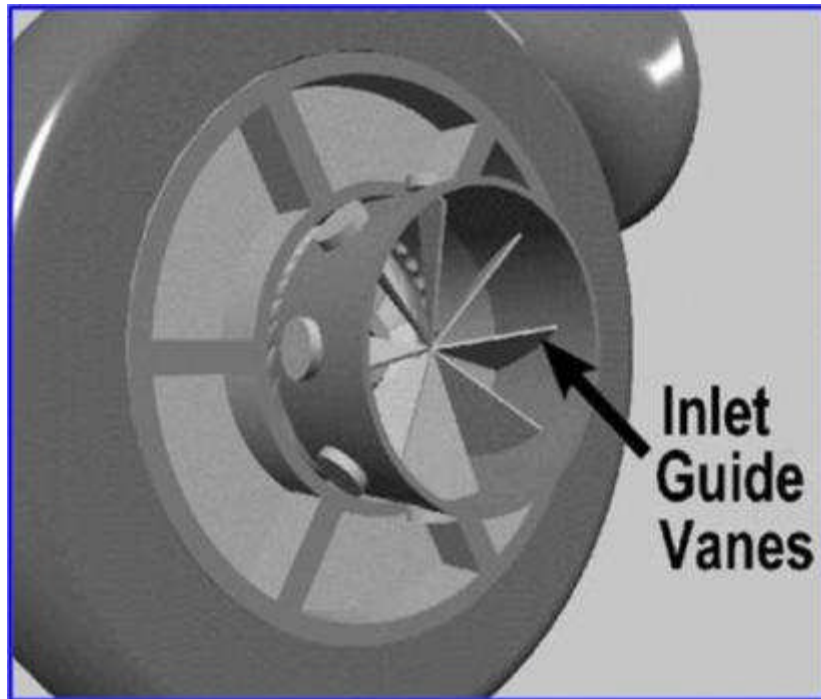


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Inlet Guide Vanes



Added at the inlet eye of impeller, called “inlet guide vane”, for capacity control

Provide inlet pressure drop

Impact wheel motion to gas, which reduces work for impeller

Increase part load stability

Closed at startup to reduce inrush current of motor at startup

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Inlet Guide Vanes

0~10% -- IGV acts as a valve/Throttling device

Above 10% -- IGV changes direction of impact of gas on impeller

Suction gas that passes the guide vanes is rotated

Rotation against direction of impeller produce greatest lift

Rotation with direction of impeller reduce lift

Lift is what controls cooler temperature

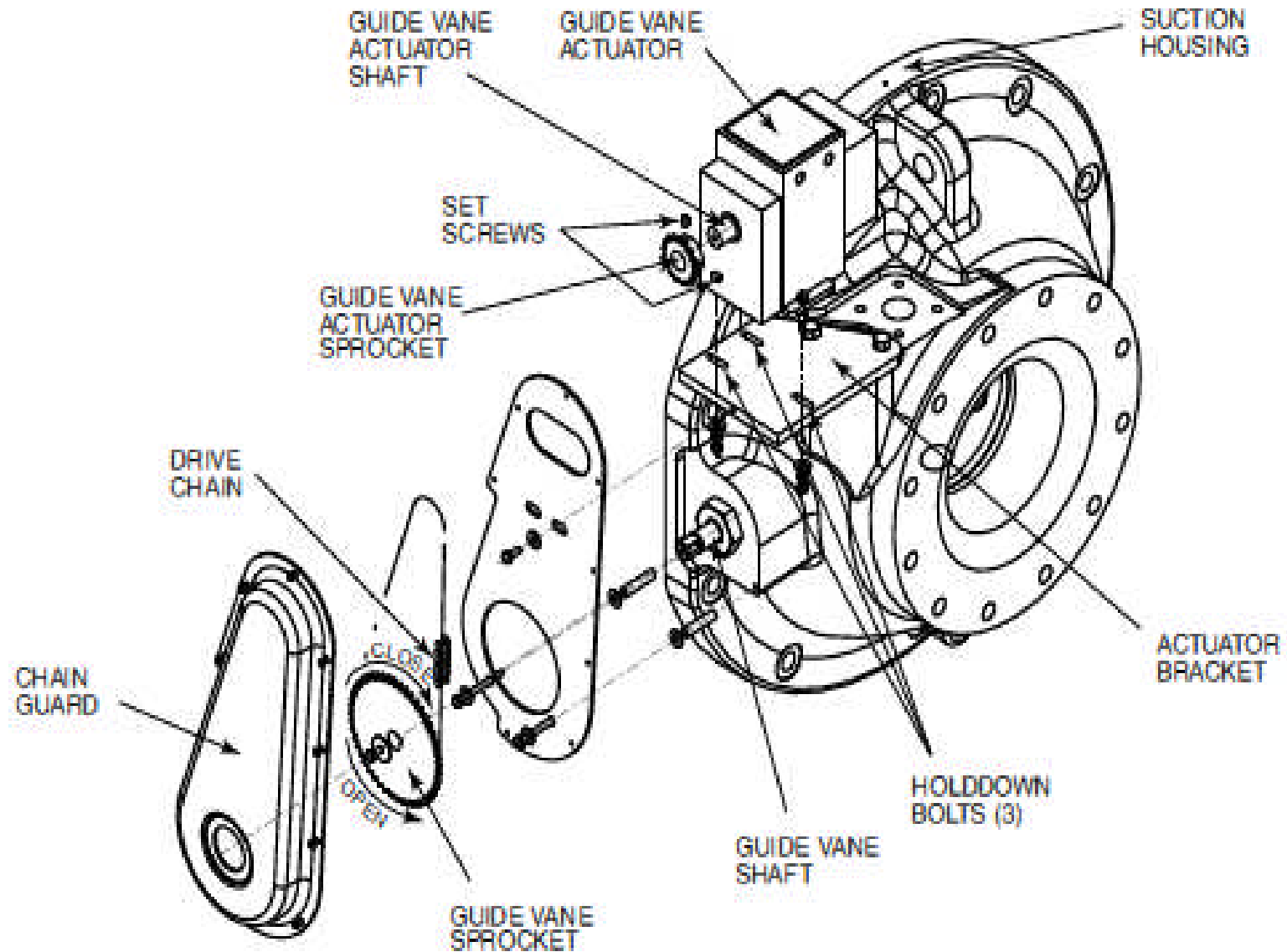
IGV opening is limited by motor current and leaving fluid temperature

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Inlet Guide Vane Assembly



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Compressor Theory

Split ring Diffuser

19XR Frame 4/5 Compressors

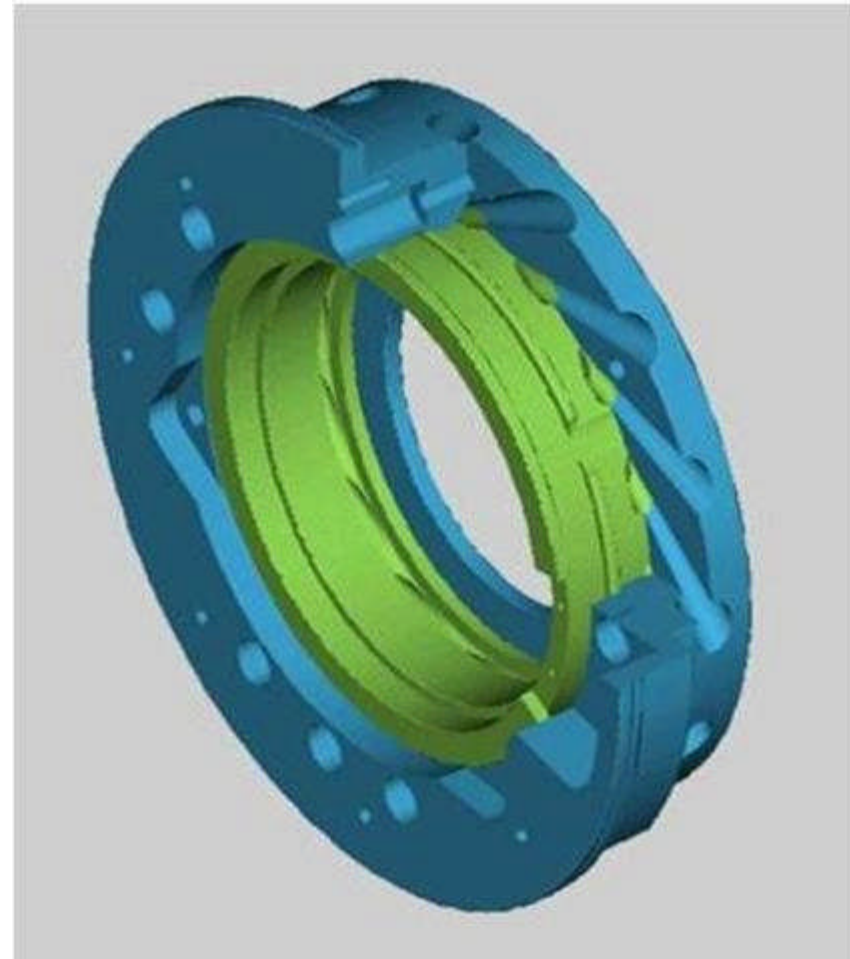
Closing – produce higher gas velocity @ discharge tip of impeller

Helps impeller produce pressure at low load

Improve efficiency and stability



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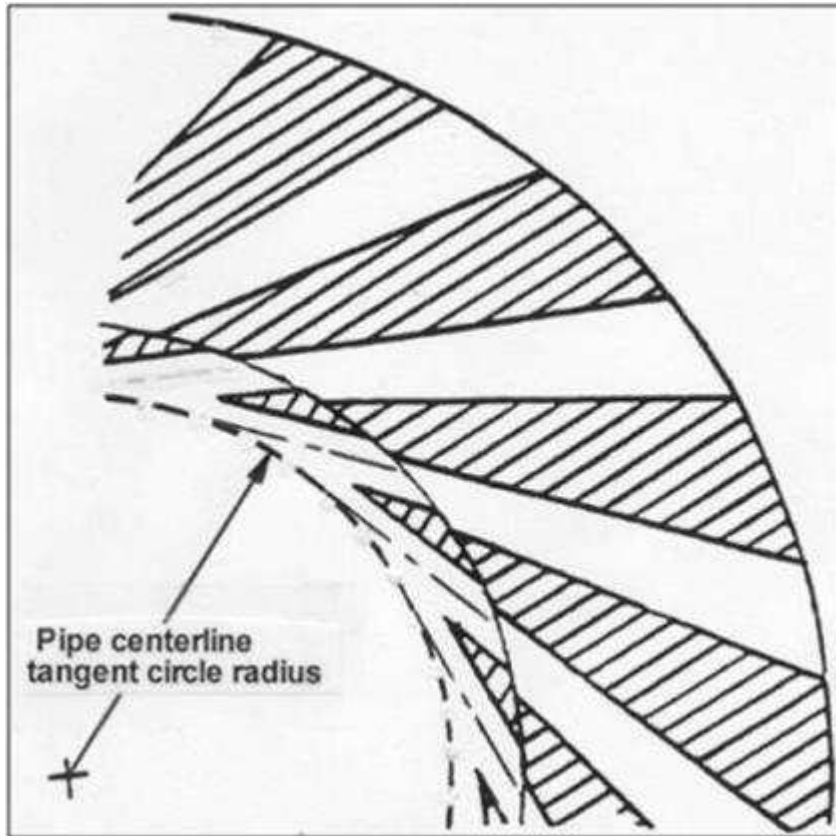


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Compressor Theory



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Closing diffuser helps the impeller by narrowing the passage through which the gas flows. In this way, the split ring diffuser helps the impeller produce pressure at low loads, thus improving efficiency and stability

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Compressor Theory



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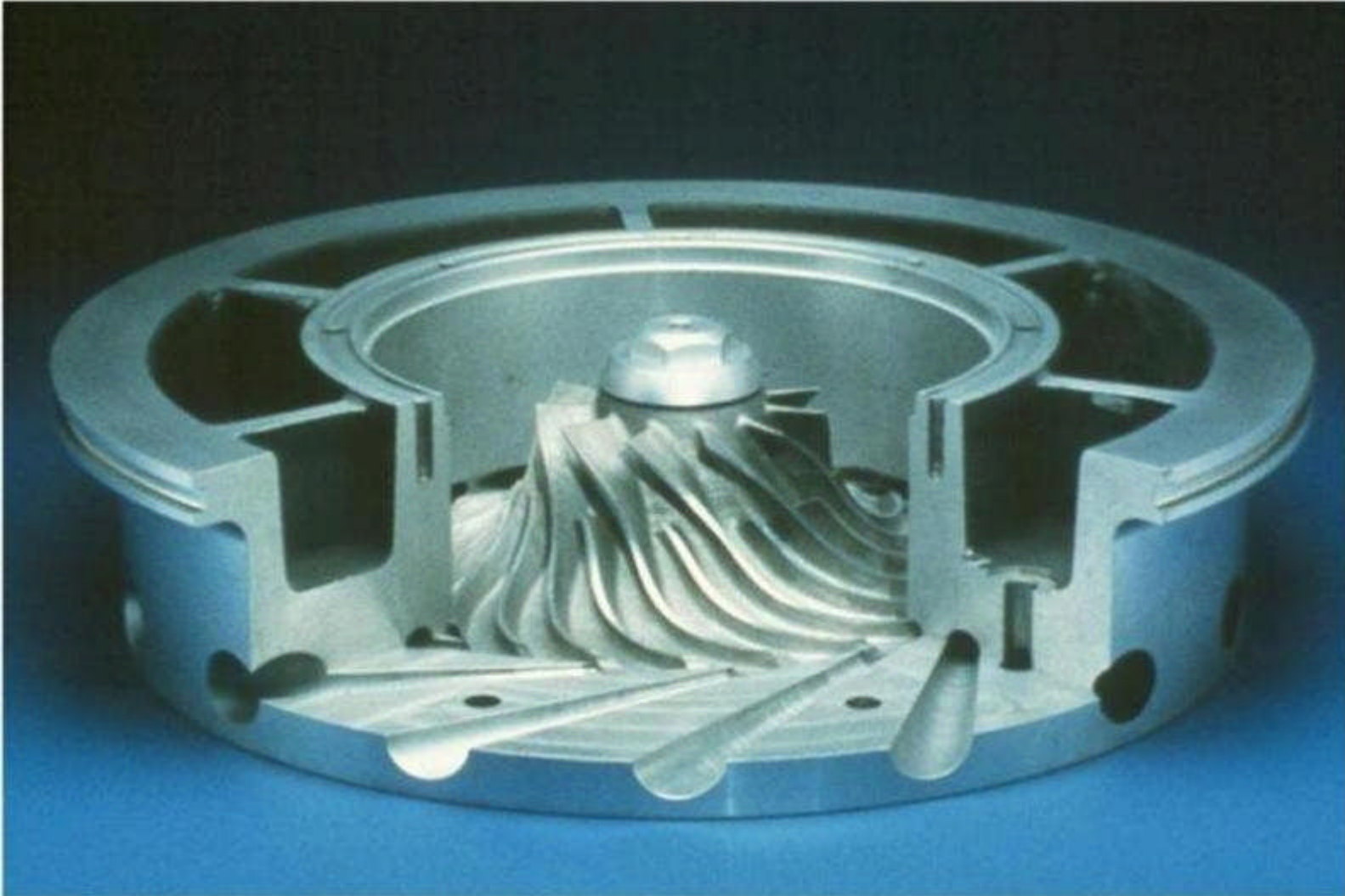


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Compressor Theory



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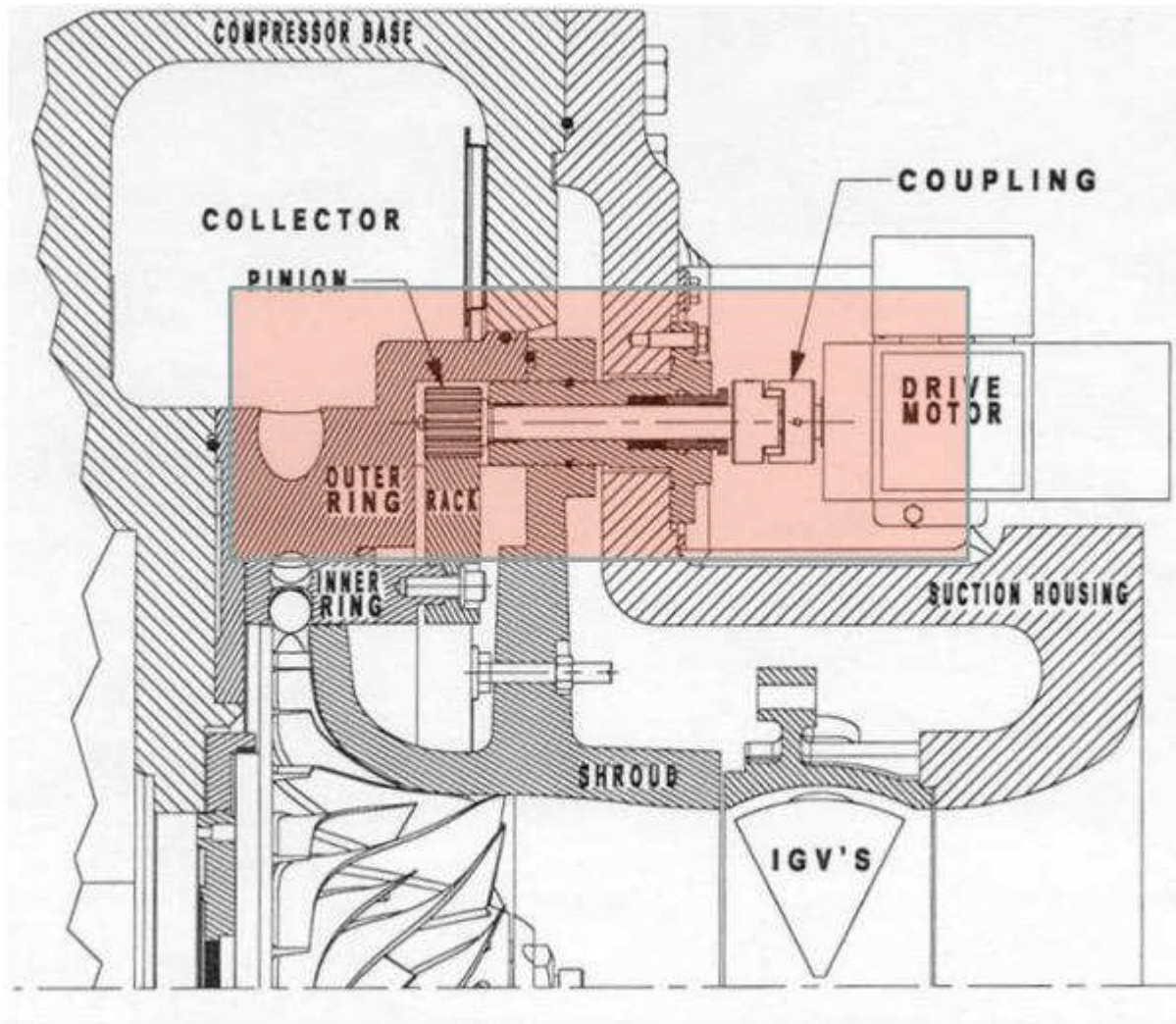


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Diffuser Actuator



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**19XR
Frame 4 & 5
Compressor
s Only**

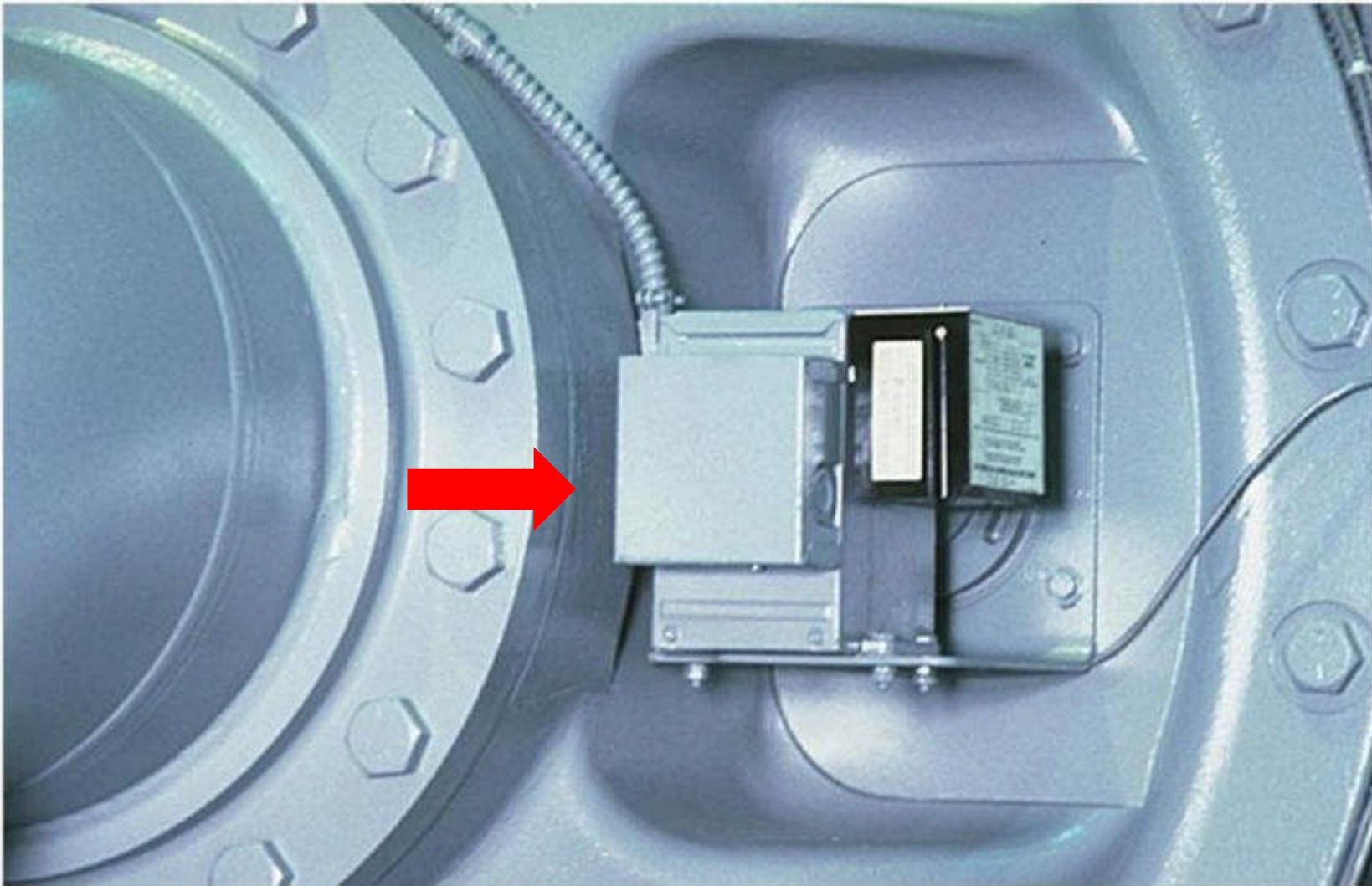
Compressor Cross section

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Diffuser Actuator



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Rotating Stall Transducer



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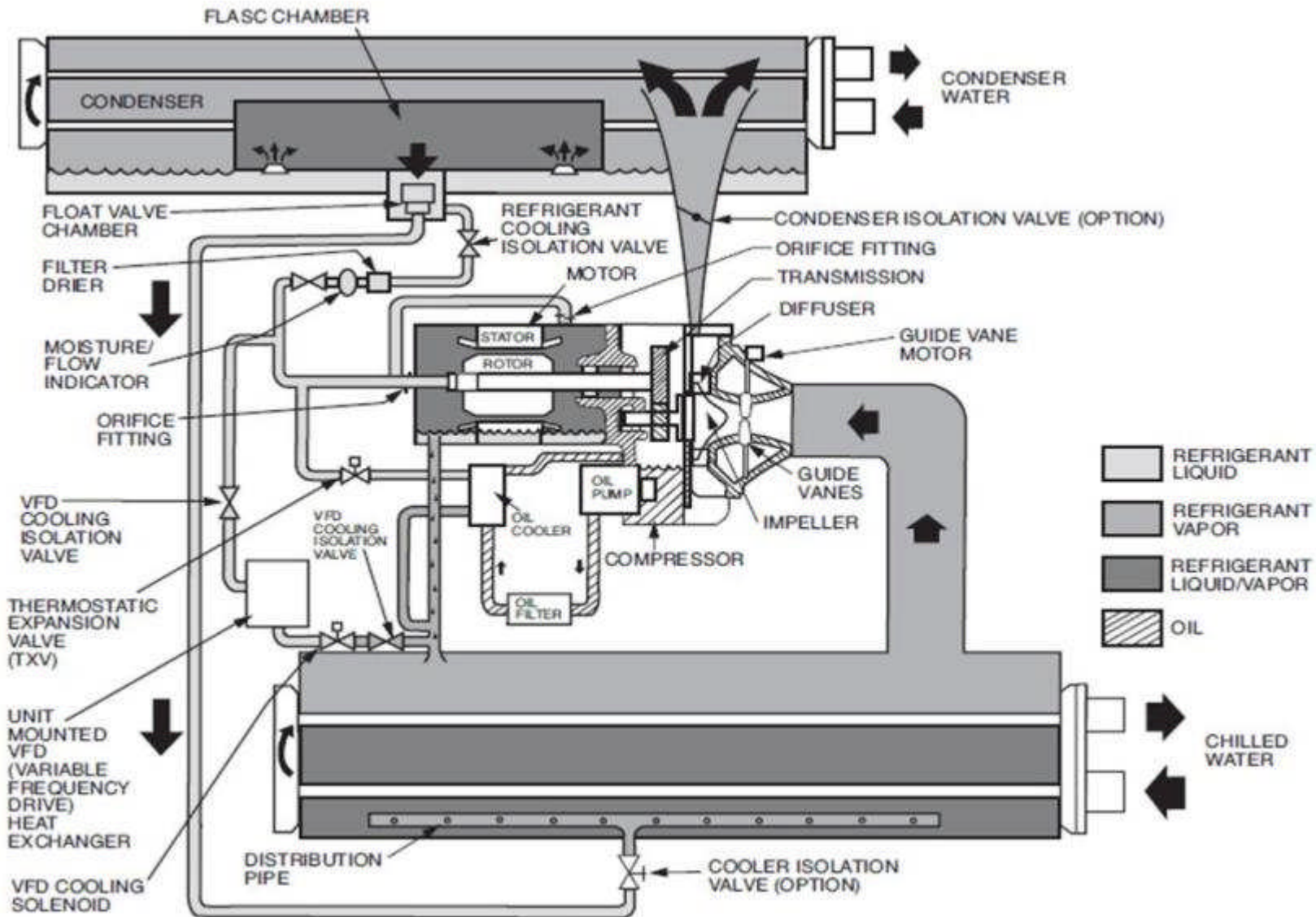


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Refrigeration Cycle



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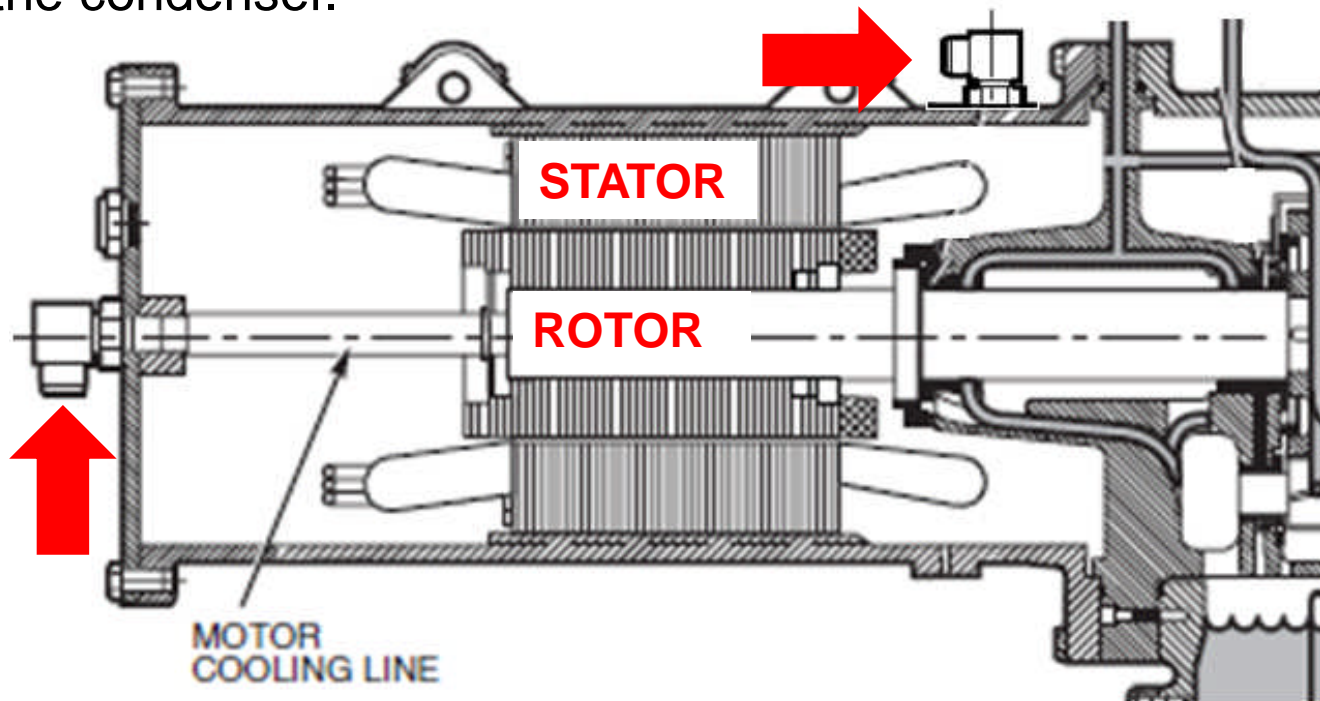
Motor cooling

The motor is refrigerant cooled.

Liquid is injected into the dam located on the rotor and travels through slots in the rotor to cool stator.

Liquid is sprayed on the end turns by a fitting located on top of the stator housing.

The refrigerant is filtered through a drier with isolation valves located on the bottom of the condenser.



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Motor Thermistors



The stator contains two 5K thermistors to sense motor temperature.

These thermistors are located on the motor end turns next to the transmission. One of the thermistors is a spare.

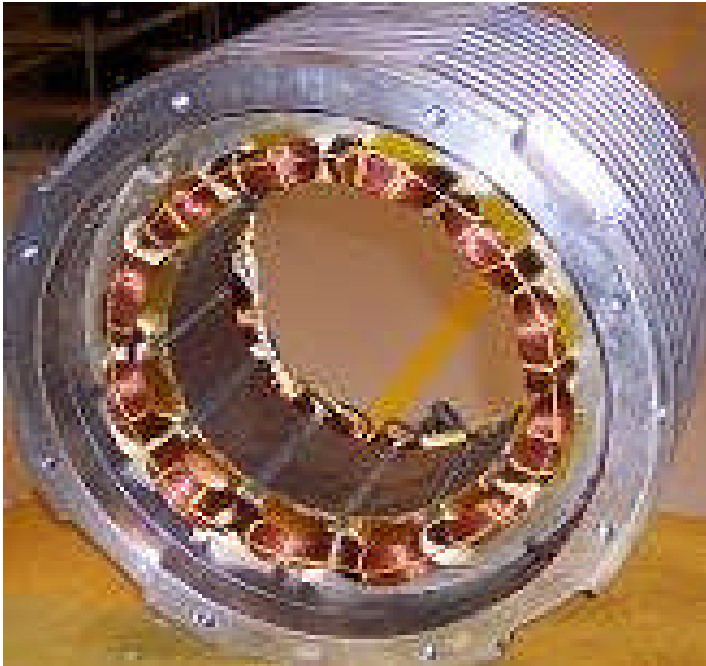
The motor area is vented to the evaporator, so it typically operates at 40-70°F.

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Two Motor Designs on 19XR



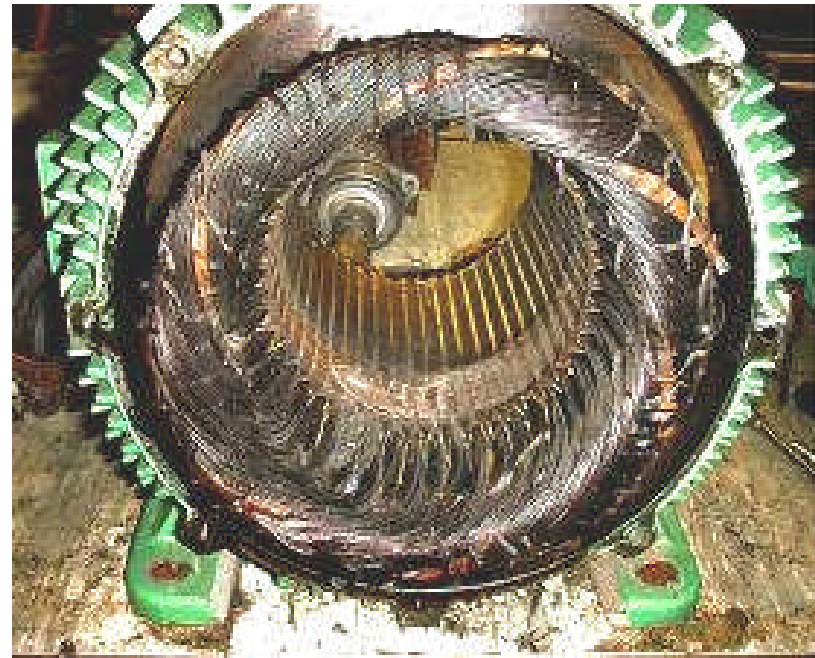
Form Wound

Winding individually formed and placed into stator slot.

Used in High voltage (2300V and above)

Better insulation on high voltage

Frame 5 only



Random Wound

Standard type of stator winding used in motors under 1000 volts

Frame 2-4

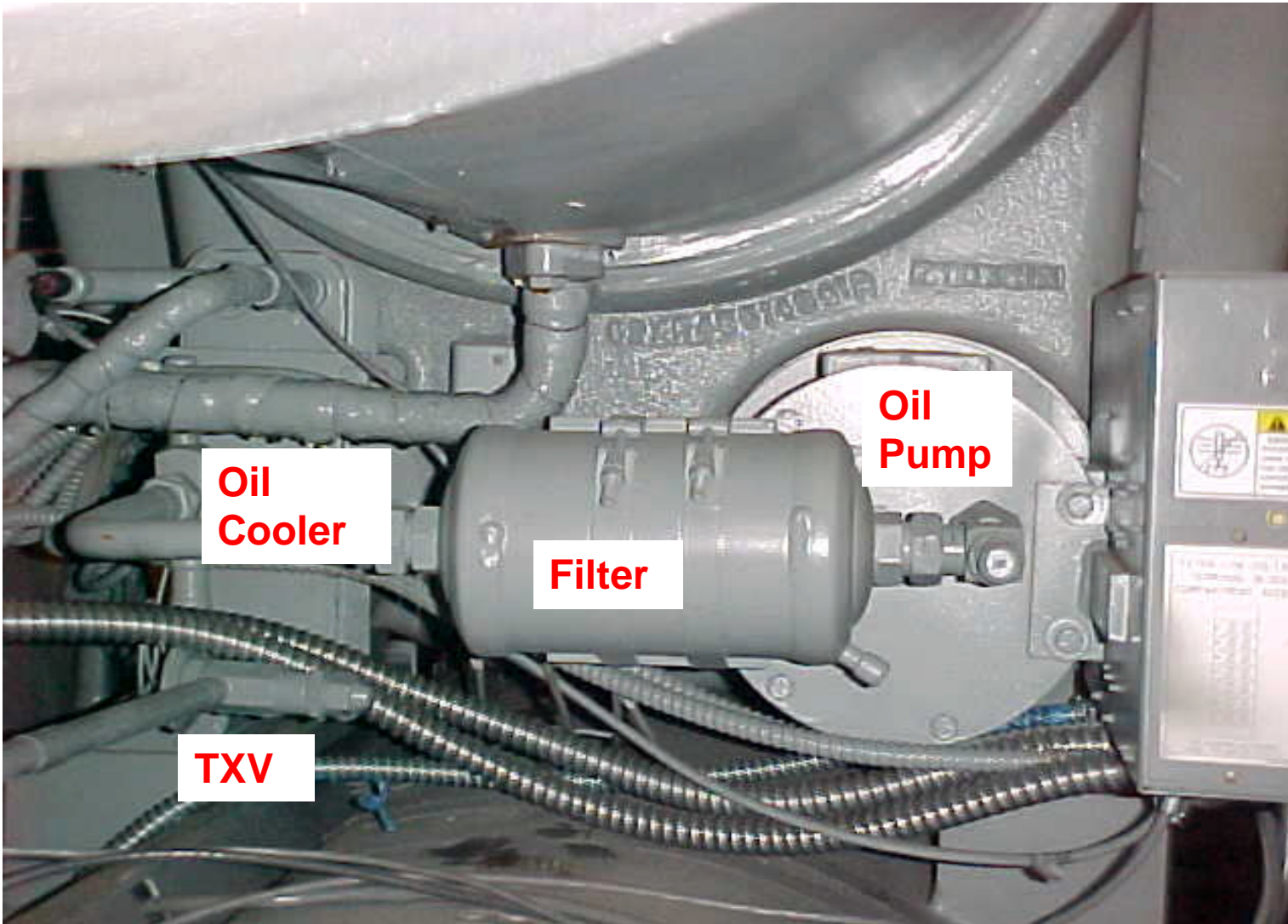
Frame 5 (sometimes)

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Lubrication



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Lubrication

The oil pump is a vane type design that is positive displacement.

15 micron filter is located on the discharge of the pump.

It provides lubrication to the two low speed bearings and the high speed assembly. The pressure is regulated by a relief valve in the Oil sump.

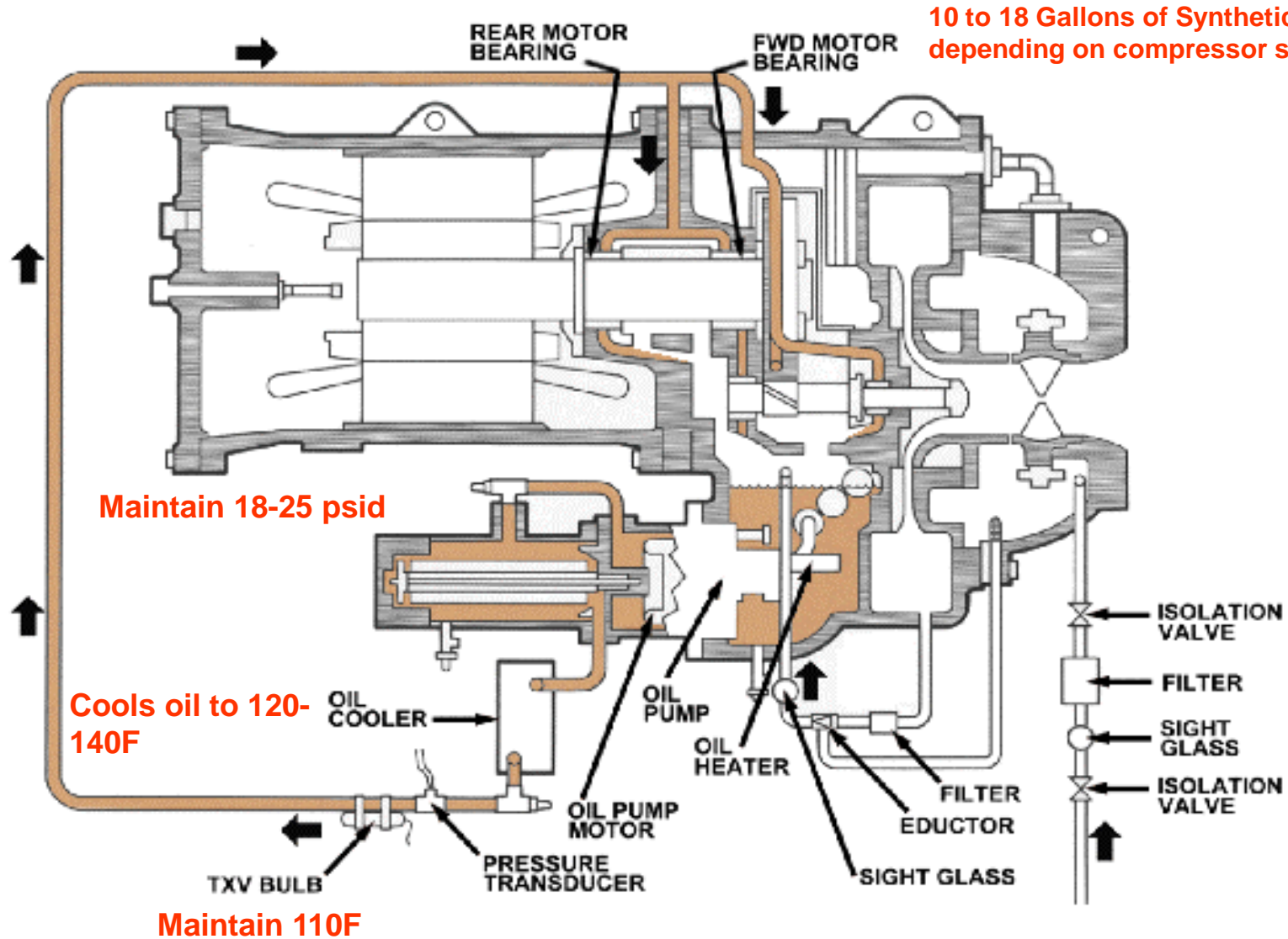
The temperature is regulated by a refrigerated oil cooler that maintains 110-120 degree f leaving oil temperature. With the system off, the oil heater maintains a temperature Of 140 degree f.

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Lubrication



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Lubrication

Oil Temp

Operating = between 125°F and 150°F

Shutdown



a) energize heater if sump < 140°F or sump < cooler refrigerant temp + 53°F

b) de-energize heater if sump > 152°F or > 142°F and > cooler refrigerant temp +55°F

Start-up Delay = if Oil temp - Evap refrig temp is 50°F or less, then startup is delayed until 50°F or greater.

NOTE: Oil heater is OFF during start-up or during compressor run.

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Lubrication (continue)

Oil Pressure

Oil Pressure Relief valve maintains 18–30 psid or 18-40 psid for rolling element bearings

Oil Discharge Press. - Oil Sump Press. (transducers)

NOTE: If Oil Pressure < 15 PSID, then compressor will shutdown.

Oil Pump

@ Start-up = energizes providing 45 sec of pre-lube to bearings after pressure verification.

During Shutdown = continues to operate for 60 sec for post-lube.

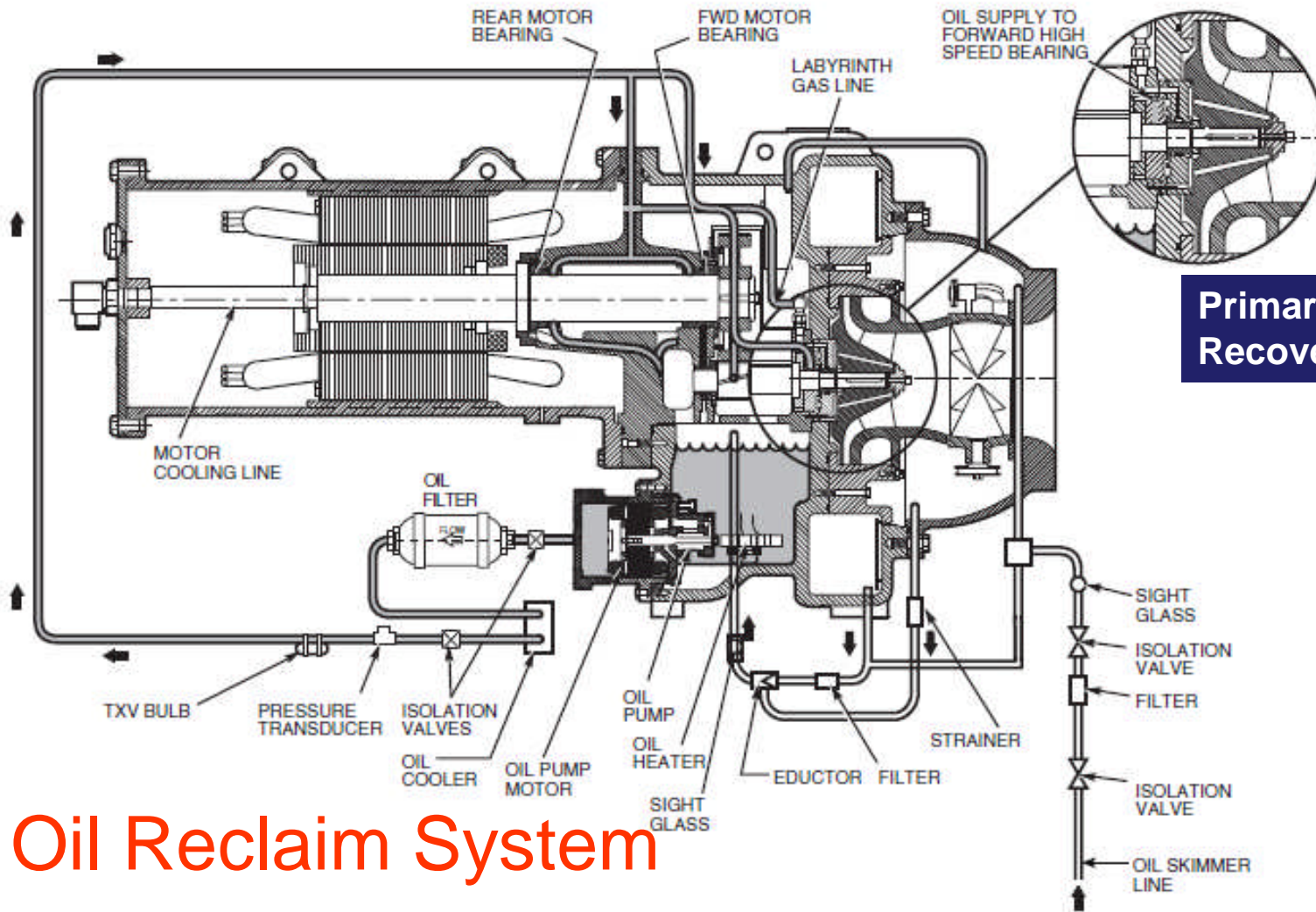
Shutdown = energizes for 30 sec for every 30 mins that the oil heater is energized to stir oil sump and therefore reduce refrigerant entrained in oil.

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Compressor Oil Recovery



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Primary Oil Recovery

Oil Reclaim System

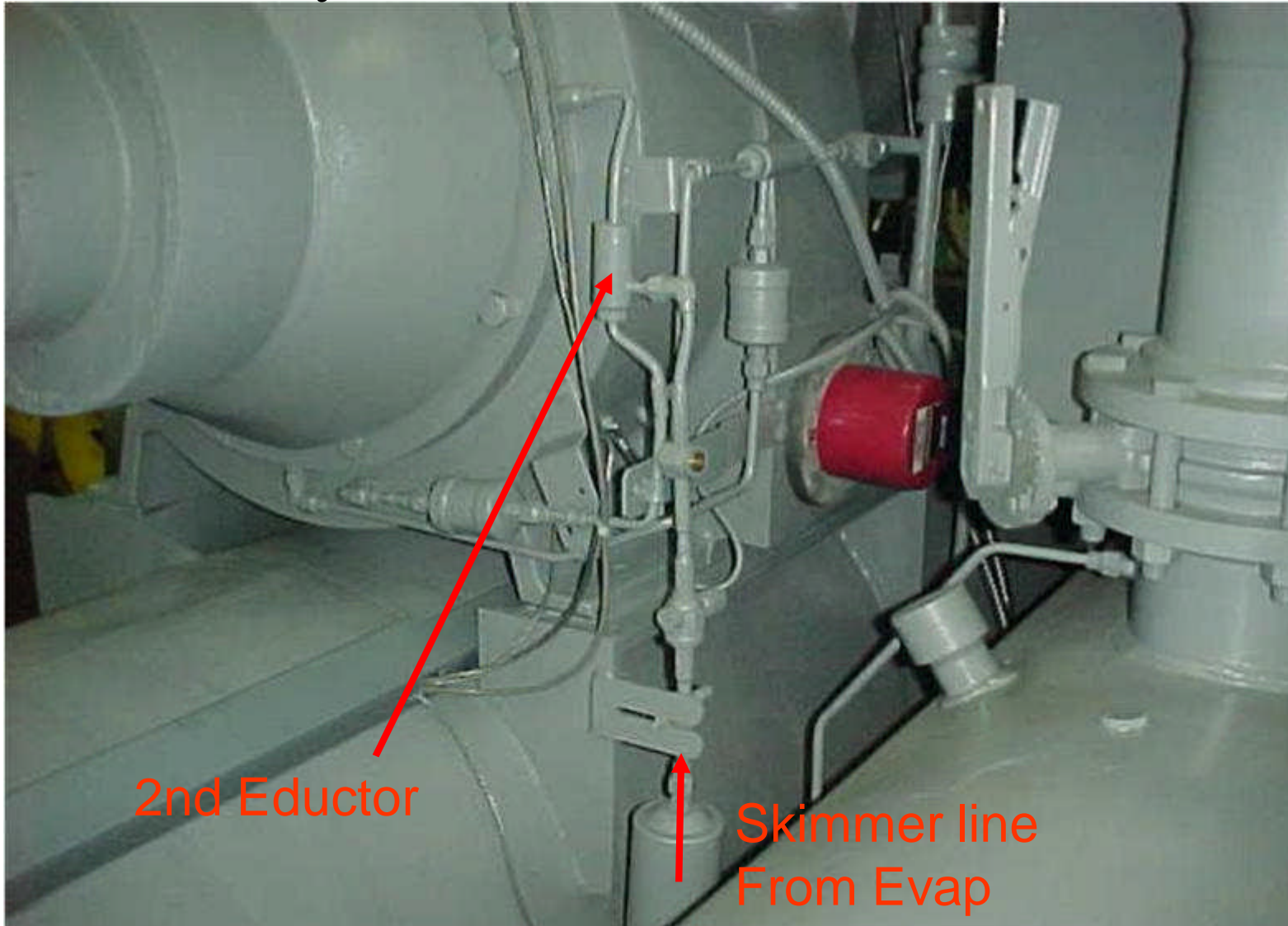
Secondary Oil Recovery

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Oil Recovery NEW DESIGN dual eductor

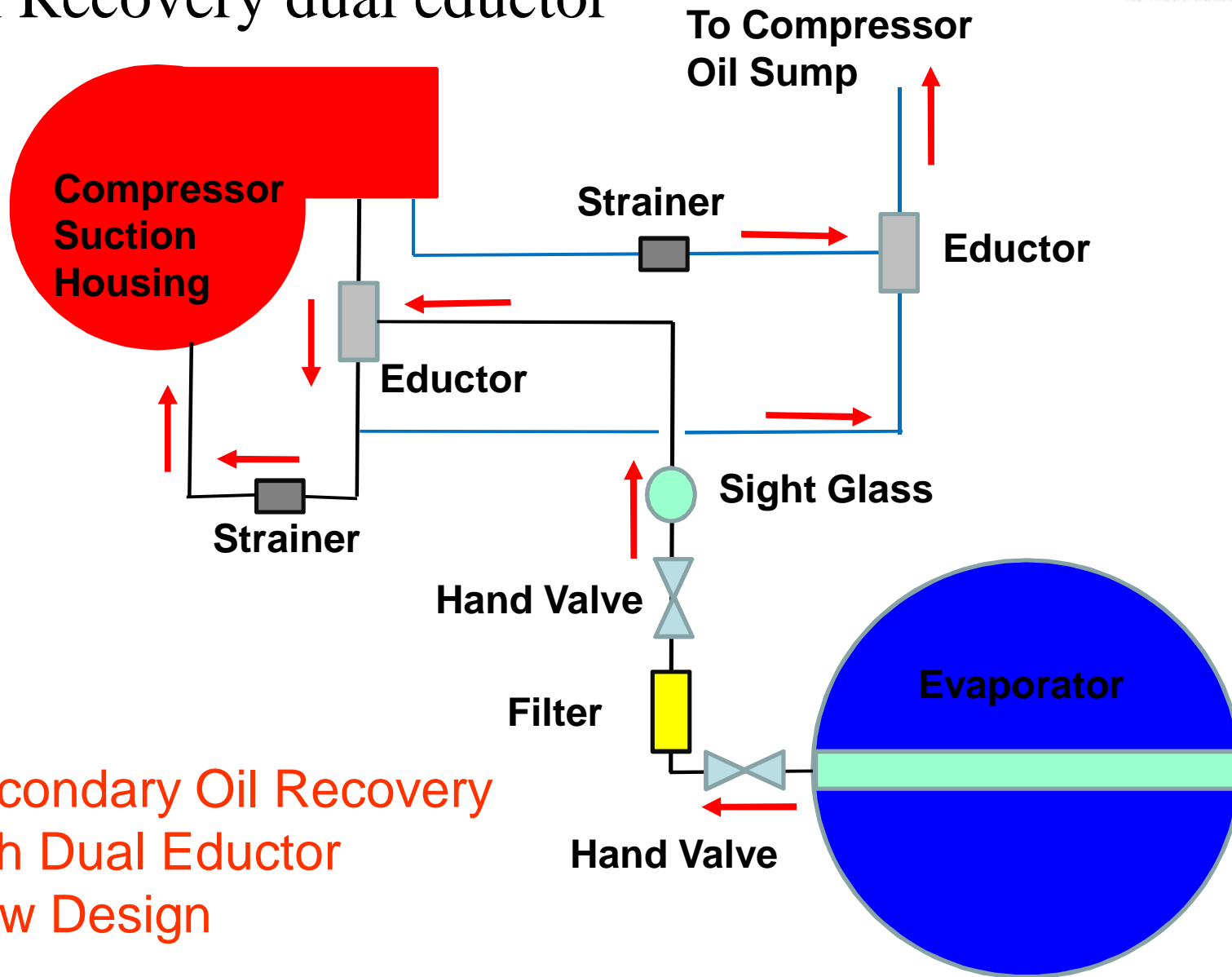


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Oil Recovery dual eductor



Secondary Oil Recovery
with Dual Eductor
New Design

19XRV



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Oil Recovery NEW DESIGN dual educator

	OLD	NEW (Dual Educator)
Primary Oil Recovery Mode	Oil travel with refrigerant into suction housing where educator transports recovered oil to oil sump from suction housing	SAME
Secondary Oil Recovery Mode	Under <u>ANY</u> conditions oil/refrigerant mixture is removed from top of liquid level in evaporator by educator. Oil/refrigerant mixture is carried to suction housing where educator transports mixture to oil sump	Under <u>LIGHT LOAD conditions</u> (IGV closed creating pressure differential) causing oil/refrigerant mixture to be removed from top of liquid level in evaporator. Oil/refrigerant mixture is carried to suction housing where educator transports mixture to oil sump

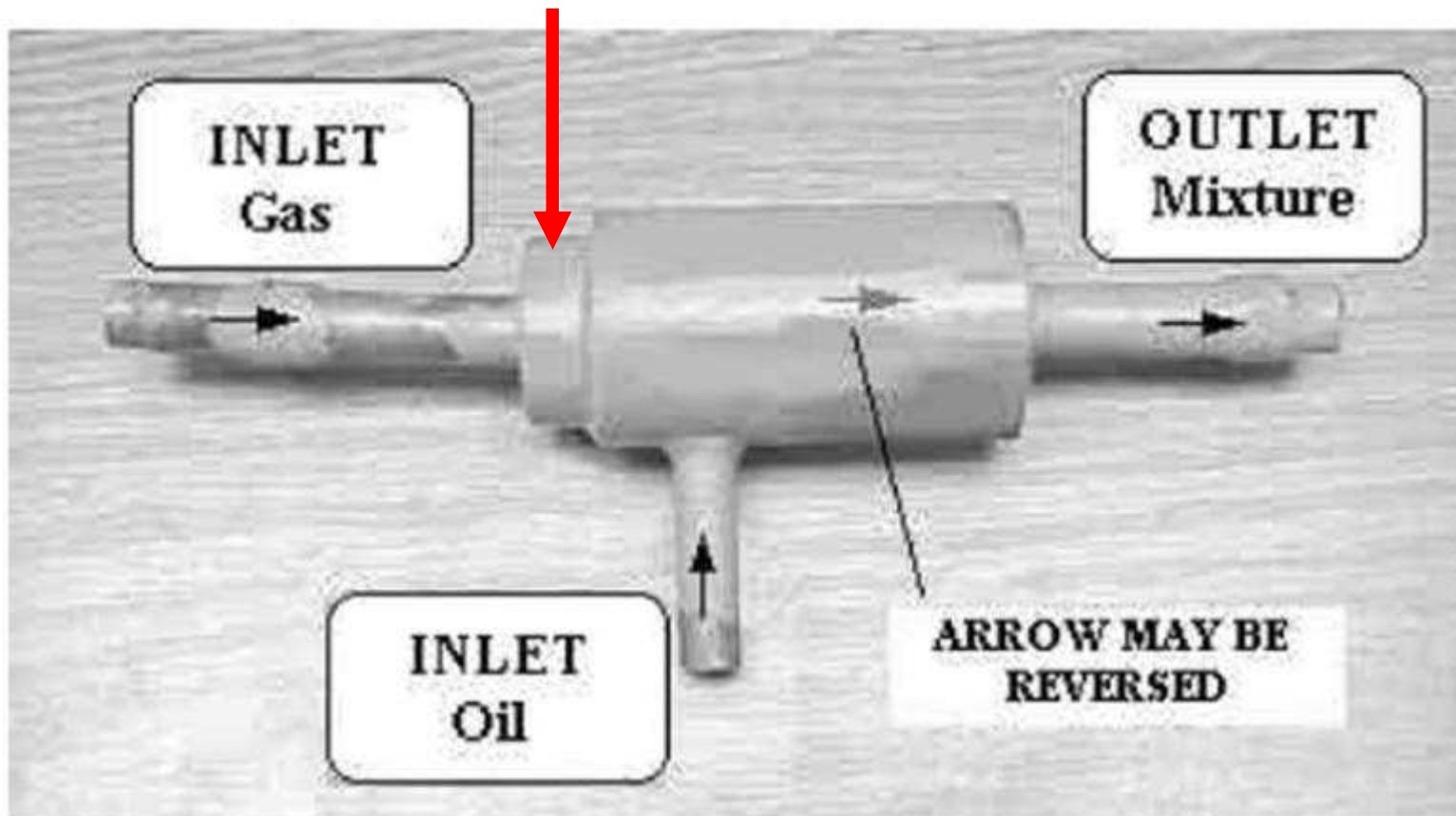
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Eductor – Correct flow

Small diameter
is Inlet side



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Lubrication

Oil Level

Operating = visible in one of two sight glasses

Shutdown = visible between middle of upper glass and top of lower.



**Maximum oil level when
not running**

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High Speed Bearings



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Kingsbury thrust design



Rolling element bearing

- On all Frame 3 compressor starting sometime mid-2001. Call engineering to check
- Frame 4 compressor starting week 25 2011 (see bulletin SB-C1103)
- Frame 5 compressor starting week 1 2011 (see bulletin SB-C1103)

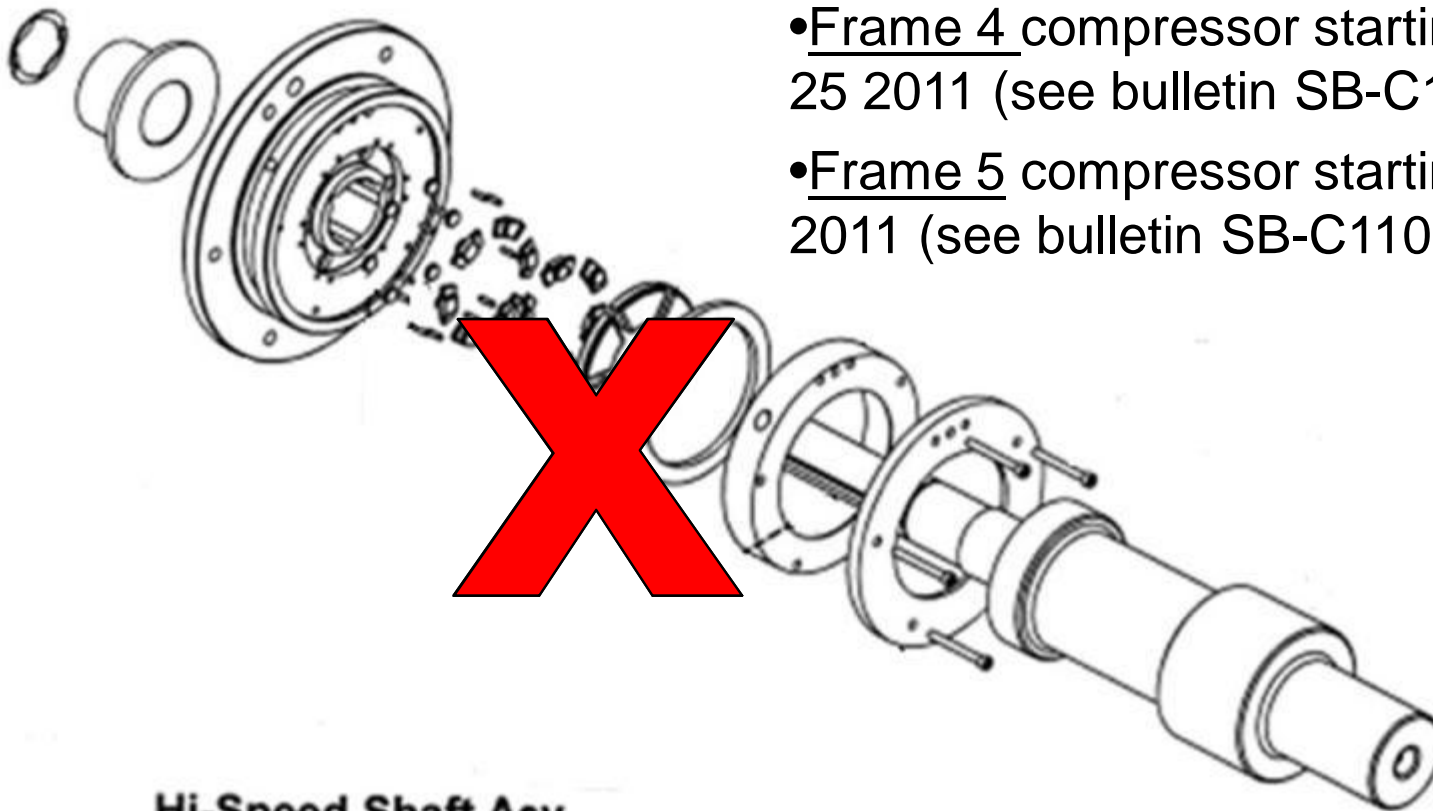
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High Speed Bearings



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- On all Frame 3 compressor starting sometime mid-2001. Call engineering to check
- Frame 4 compressor starting week 25 2011 (see bulletin SB-C1103)
- Frame 5 compressor starting week 1 2011 (see bulletin SB-C1103)



Hi-Speed Shaft Asy

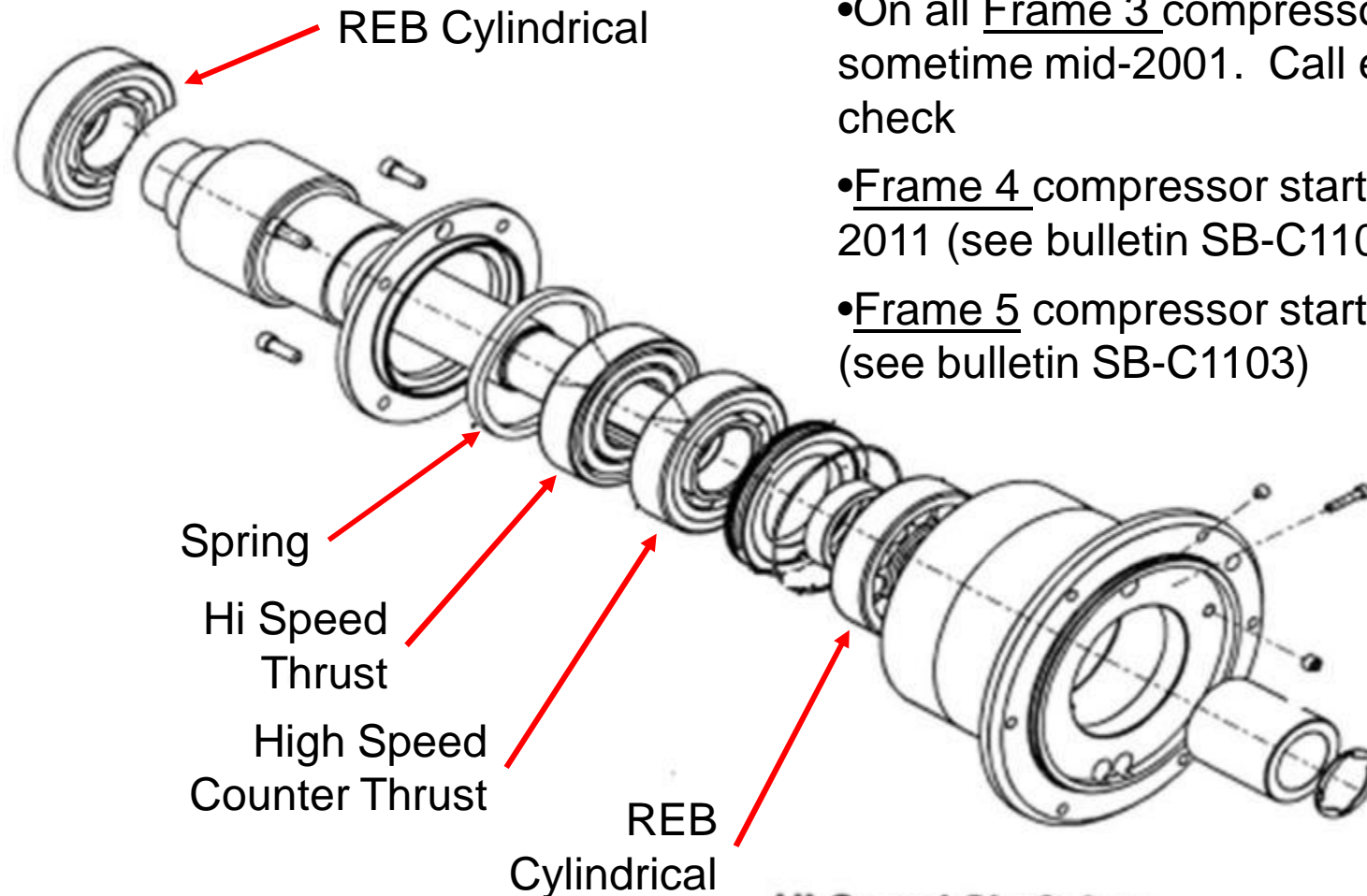
Compressors Without Roller Element Bearings

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High Speed Bearings



- On all Frame 3 compressor starting sometime mid-2001. Call engineering to check
- Frame 4 compressor starting week 25 2011 (see bulletin SB-C1103)
- Frame 5 compressor starting week 1 2011 (see bulletin SB-C1103)

Hi-Speed Shaft Asy

Compressors With Roller Element Bearings



Two types of sensors

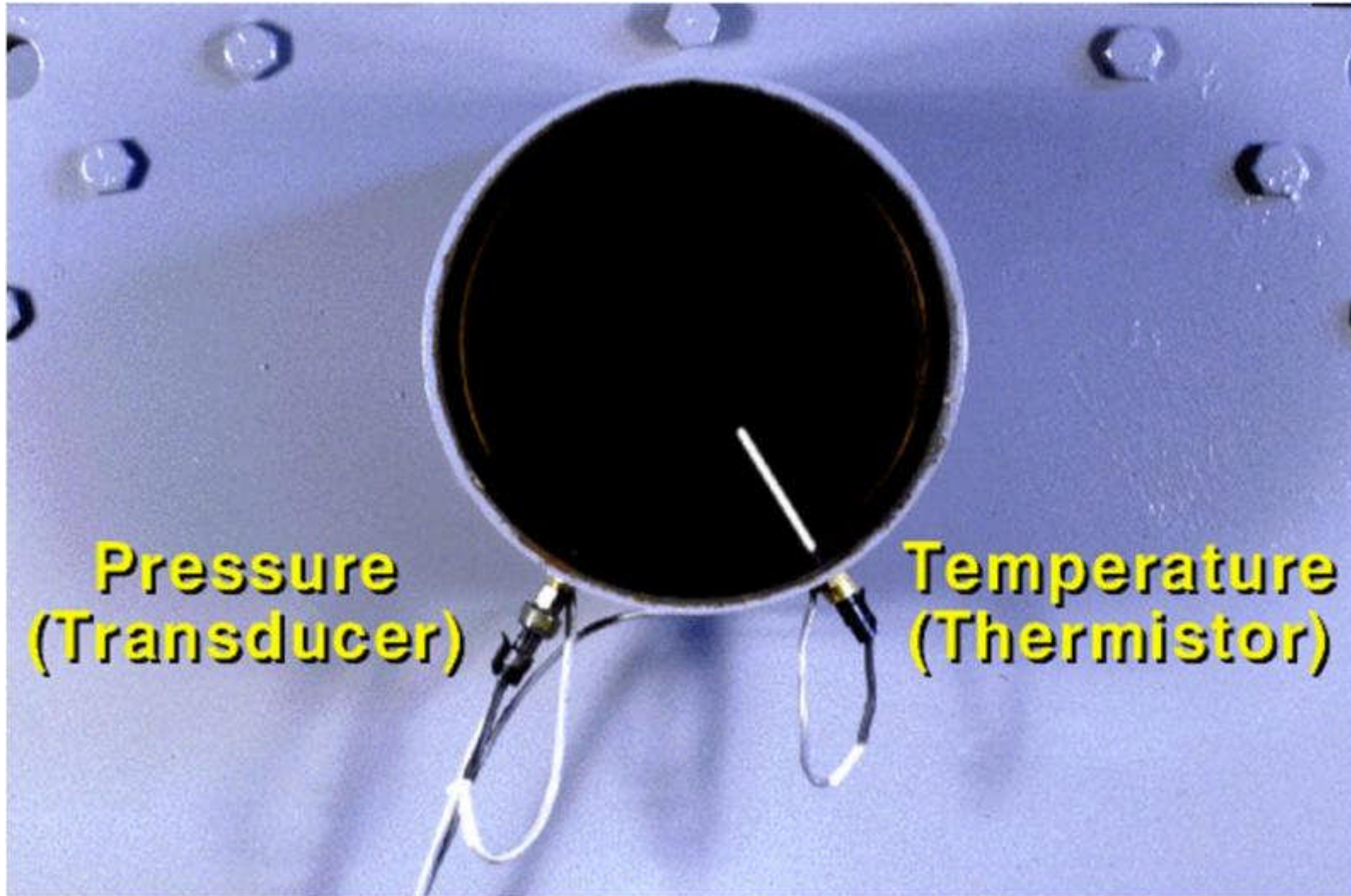
1. Temperature sensors with wells. This sensor cannot be separated from its cable, but the sensor can be removed from well without breaking into fluid boundary
2. Thermistor. This sensor is installed within compressor for motor windings or thrust bearing temp. There is 1 spare sensor

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Sensors & Transducers

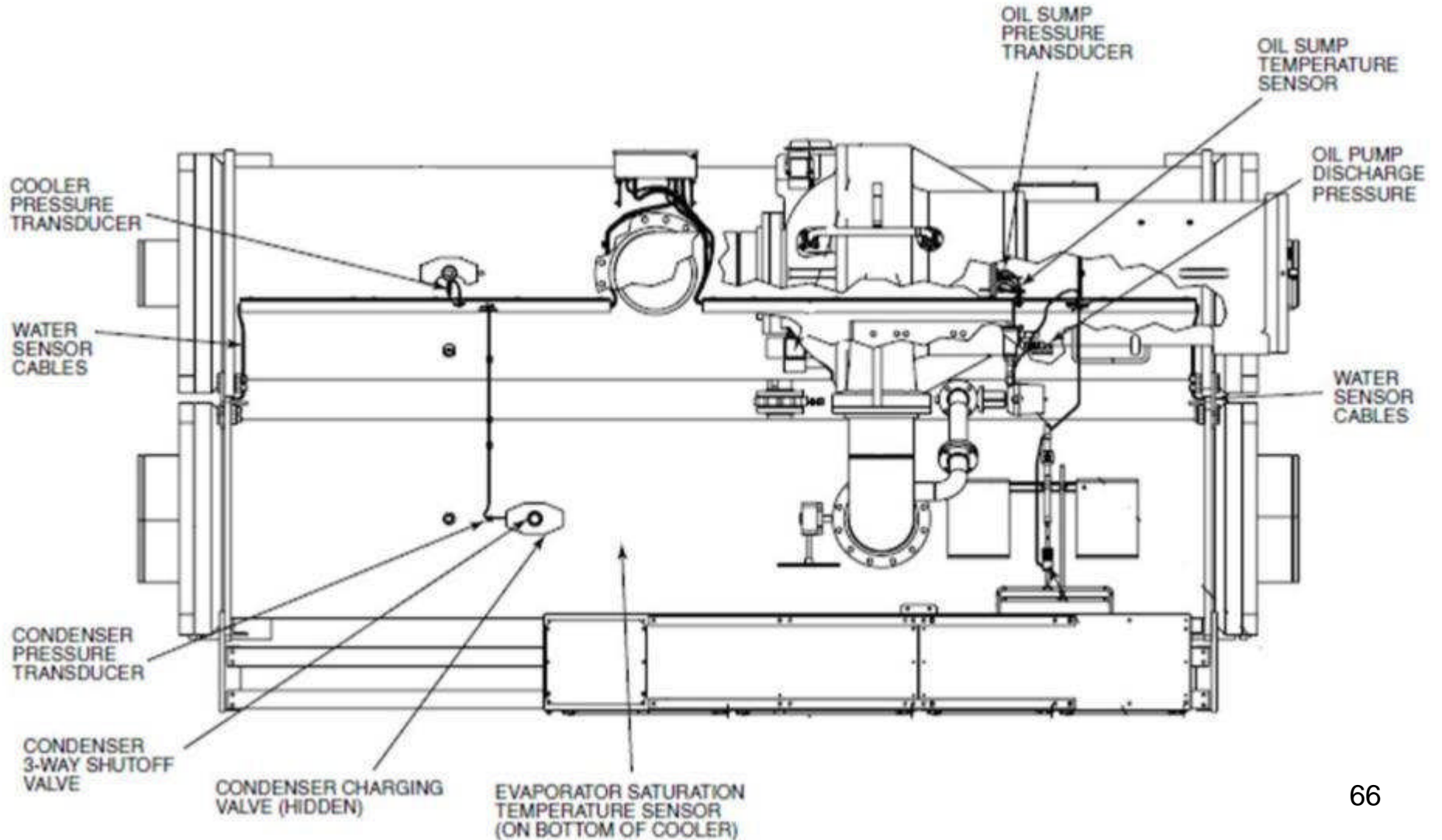


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Sensors & Transducers



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Sensors



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TYPE	LOCATION MONITORED	REMARKS
Temperature	Entering chilled water	Cooler inlet nozzle
	Leaving chilled water	Cooler outlet nozzle
	Entering condenser water	Condenser inlet nozzle
	Leaving condenser water	Condenser outlet nozzle
	Evaporator saturation	Sensor well on bottom of evaporator
	Compressor discharge	Compressor volute
	Oil sump	Compressor oil sump
	Compressor thrust bearing	Redundant sensor provided
	Motor winding	Redundant sensor provided

Total 10 temp sensors
 8 functioning sensors
 2 spares for thrust bearing and motor winding

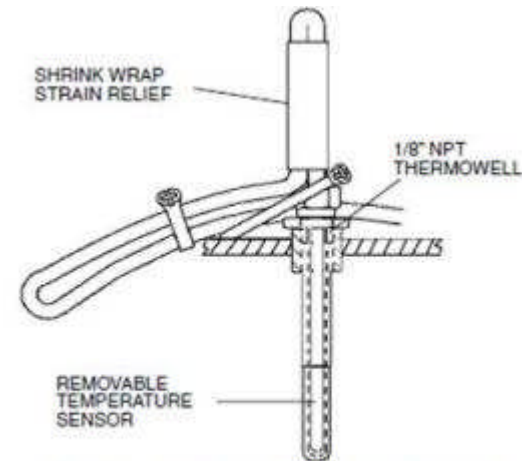


Fig. 12 — Temperature Sensor Used With Thermal Well

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Evaporator Flow

Mounted at the base of evaporator and senses refrigerant temperature directly

Uses evaporator saturation temperature in place of flow metering device

Chiller determines there is **flow** in cooler if:

- Evap saturation temp is higher than 1°F above evap refrigeration trippoint
- Evap refrigeration temp is greater than evap refrigeration trippoint

Chiller determines there is **no flow** in cooler if

- Evap saturation temp lower than 1°F below evap refrigeration trippoint
- Evap refrigeration temp < evap refrigeration trippoint and evap app > evap app alert threshold

Condenser Flow



Chiller determines there is **flow** in condenser if:

- Condenser pressure <165 psig
- Condenser pressure do not exceed configured condenser pressure override threshold by more than 5psi

Chiller determines there is **no flow** in condenser if

- Condenser pressure > 165 psig
- Condenser pressure exceeds configured condenser pressure override threshold by more than 5psi

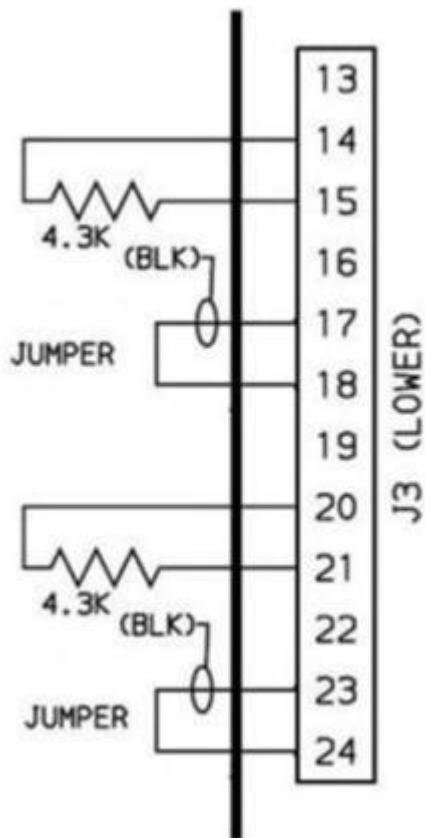
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Optional Flow Switch Wiring

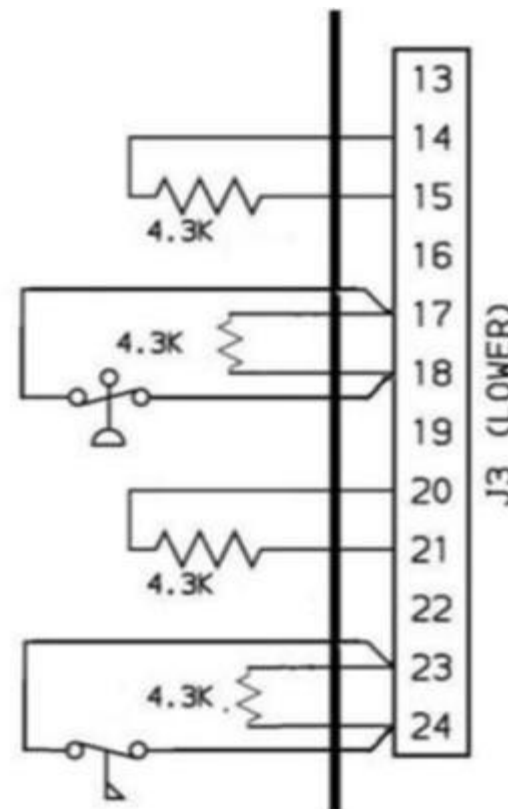


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No Flow Switches



Optional Flow Switches



CCM

***These devices are not supported by*
the chiller warranty**

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Transducers

Pressure	Evaporator	Relief valve tee
	Condenser	Relief valve tee
	Oil sump	Compressor oil sump
	Oil sump discharge	Oil pump discharge line
	Diffuser (Compressor internal)	Only in machines equipped with split ring diffusers
	Entering chilled water (Optional)	Cooler inlet nozzle
	Leaving chilled water (Optional)	Cooler outlet nozzle
	Entering condenser water (Optional)	Condenser inlet nozzle
	Leaving condenser water (Optional)	Condenser outlet nozzle
Angular Position	Guide vane actuator	Potentiometer inside of actuator
	Split ring diffuser actuator (Optional)	Potentiometer inside of actuator only on machines equipped with split ring diffusers (split ring diffuser position not displayed on ICVC)
Pressure Switch	High condenser (discharge) pressure	Compressor volute, wired into the VFD control circuit
Temperature Switch	Oil pump motor winding temperature	Wired into the oil pump control circuit

Total 5 pressure transducer

1 pressure switch

1 temperature switch

1 actuator (Frame 2,3,4 w/o split ring diffuser)

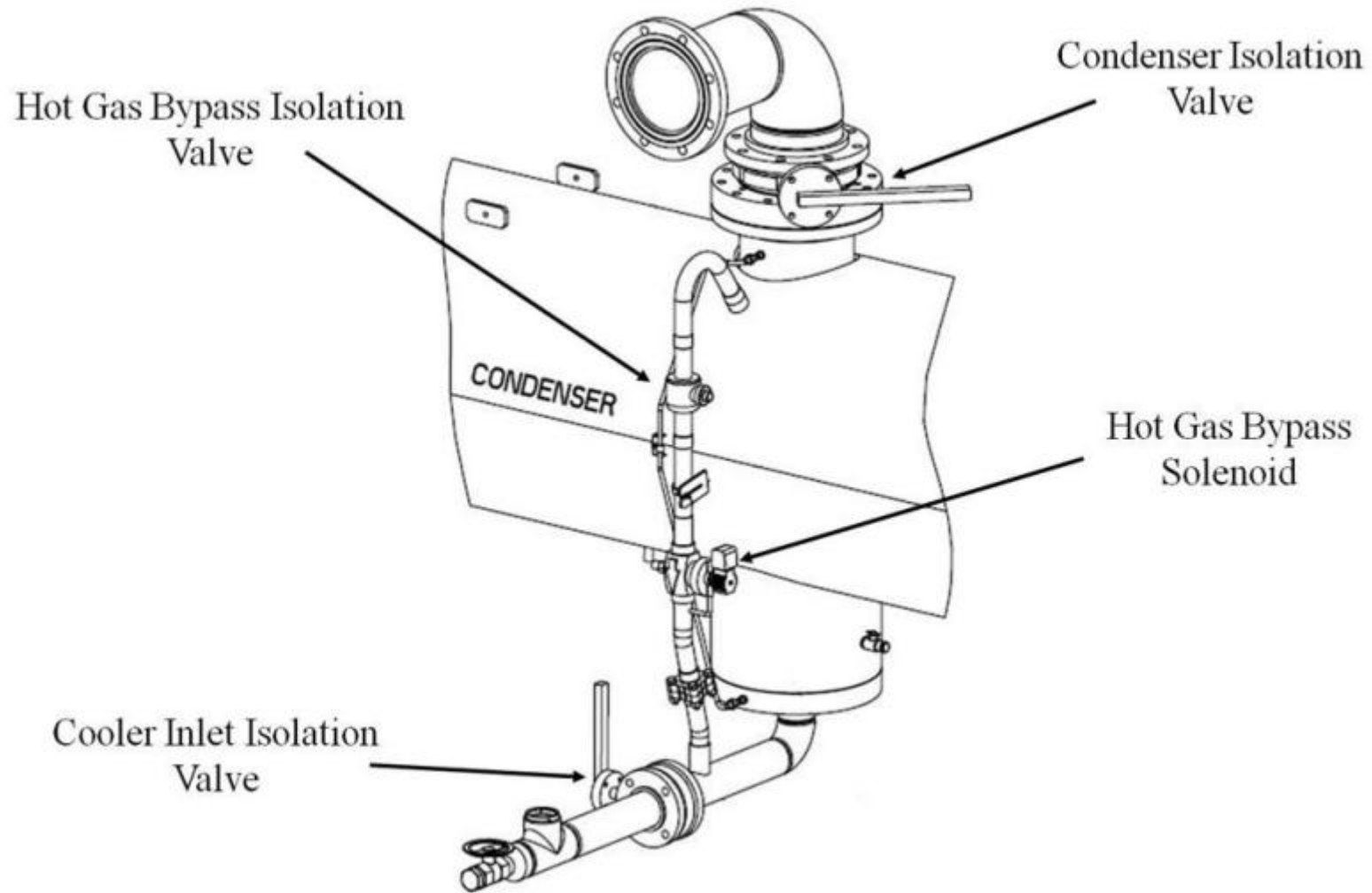
2 actuators (Frame 4 & 5 with split ring diffuser)

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Optional: Hot gas bypass



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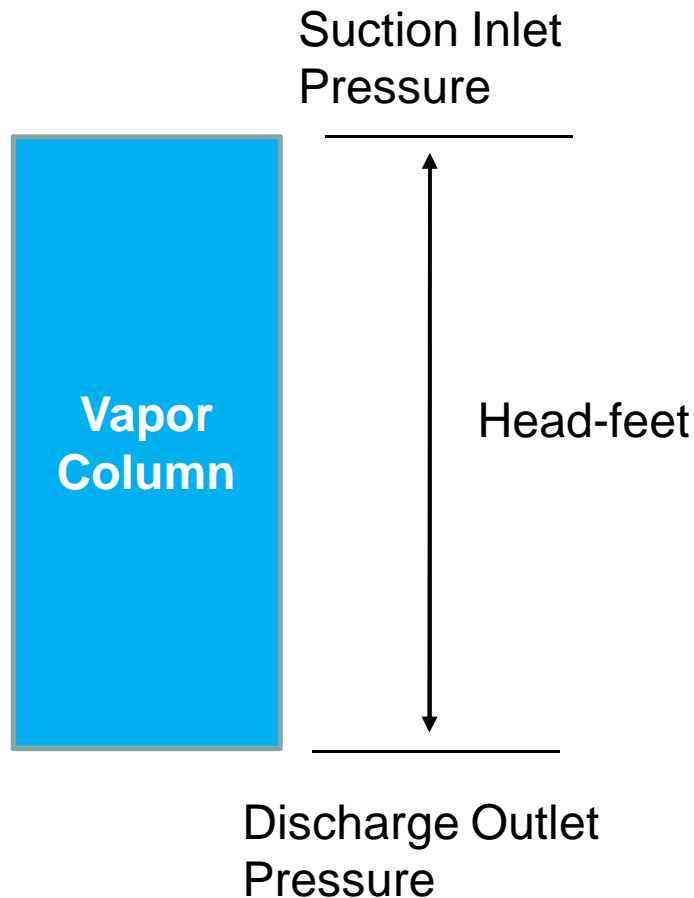
Compressor Theory

Head

Imaginary column of refrigerant vapor, measure of pressure rise developed by centrifugal compressor

Pressure at discharge minus pressure at suction

Directly affected by entering water temperature from cooling tower



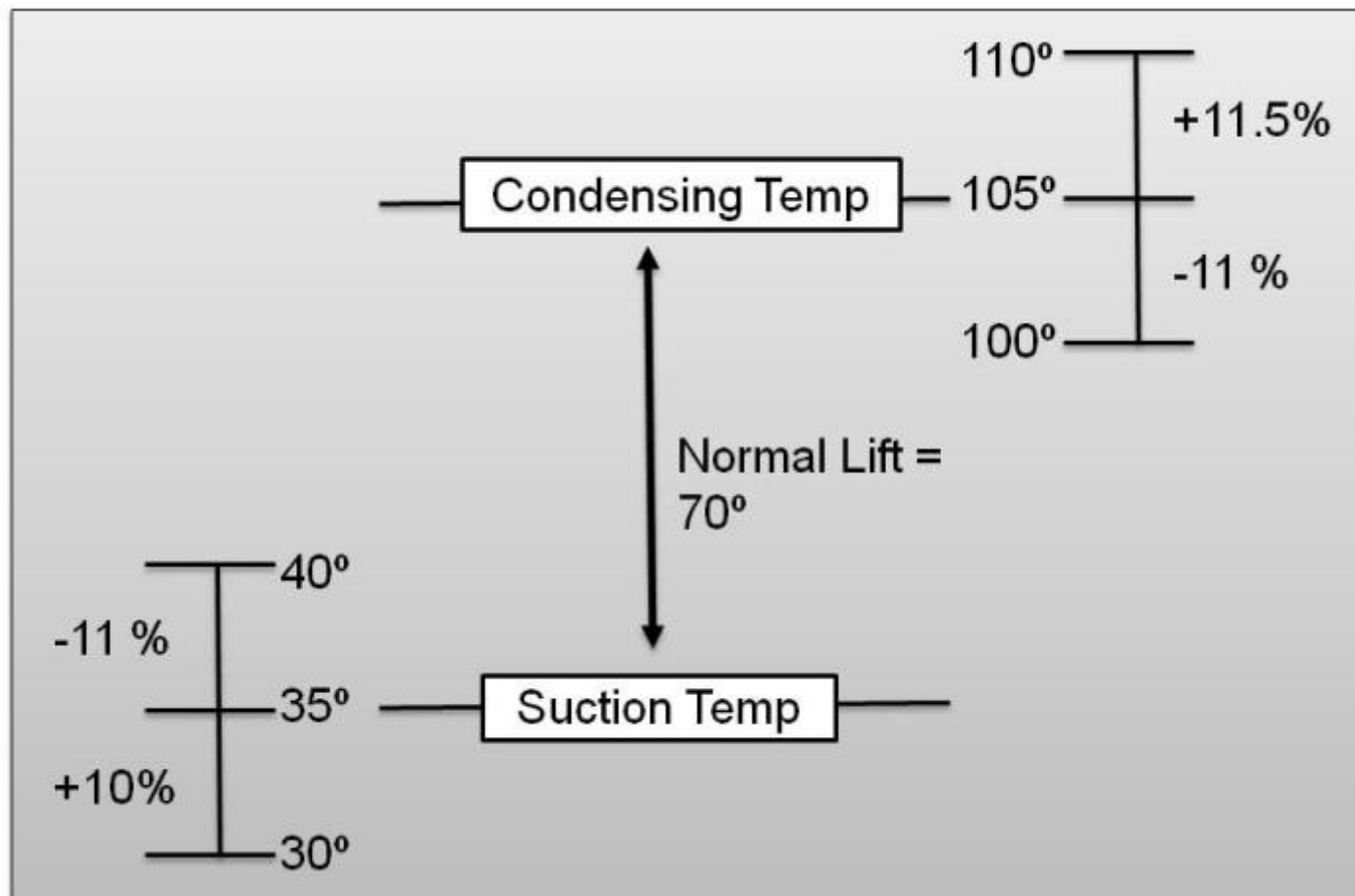
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What is Lift

Ability of compressor to lift refrigerant gas from cooler saturated suction temperature level to condenser saturated discharge temperature level, measured in °F



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Compressor Theory



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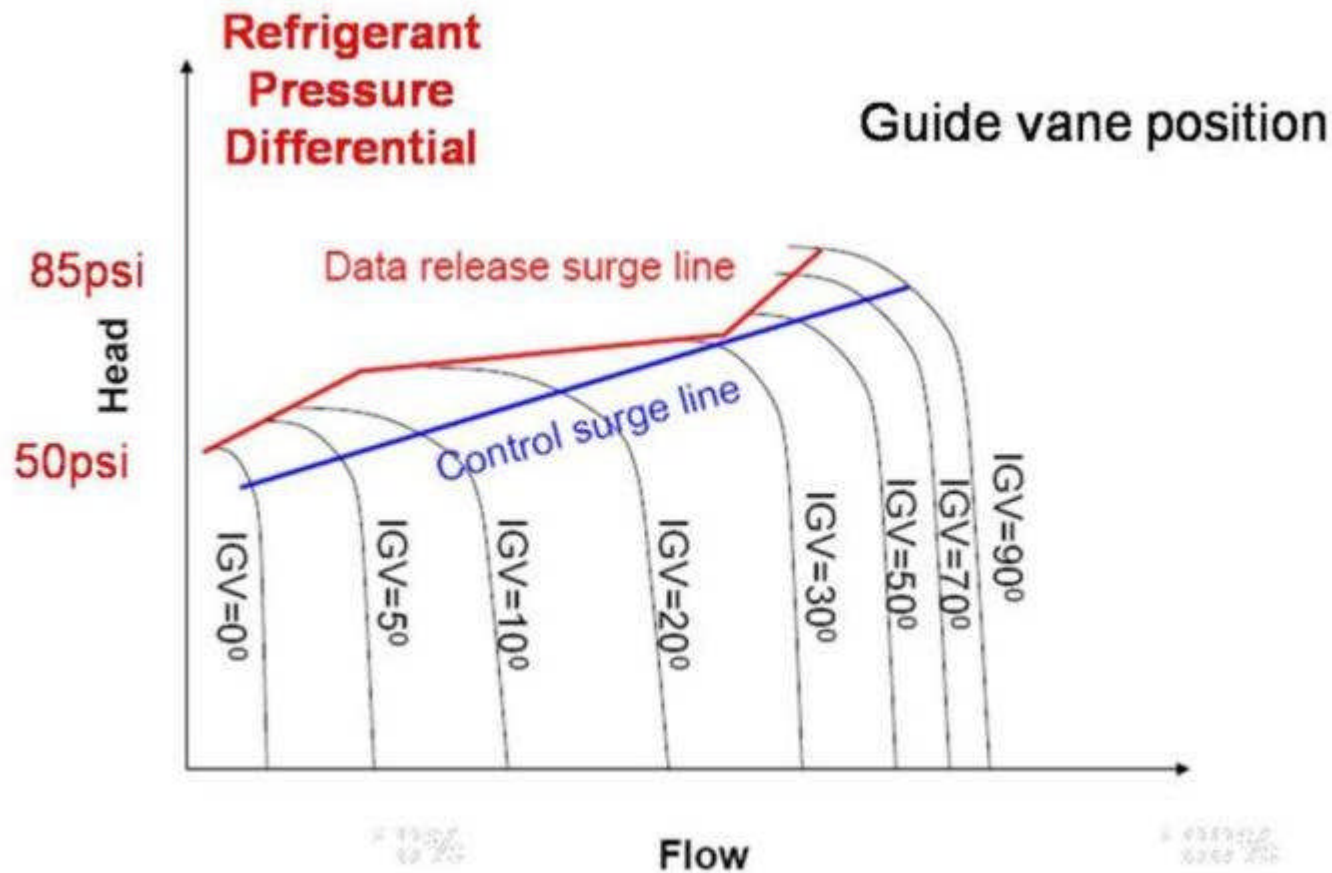
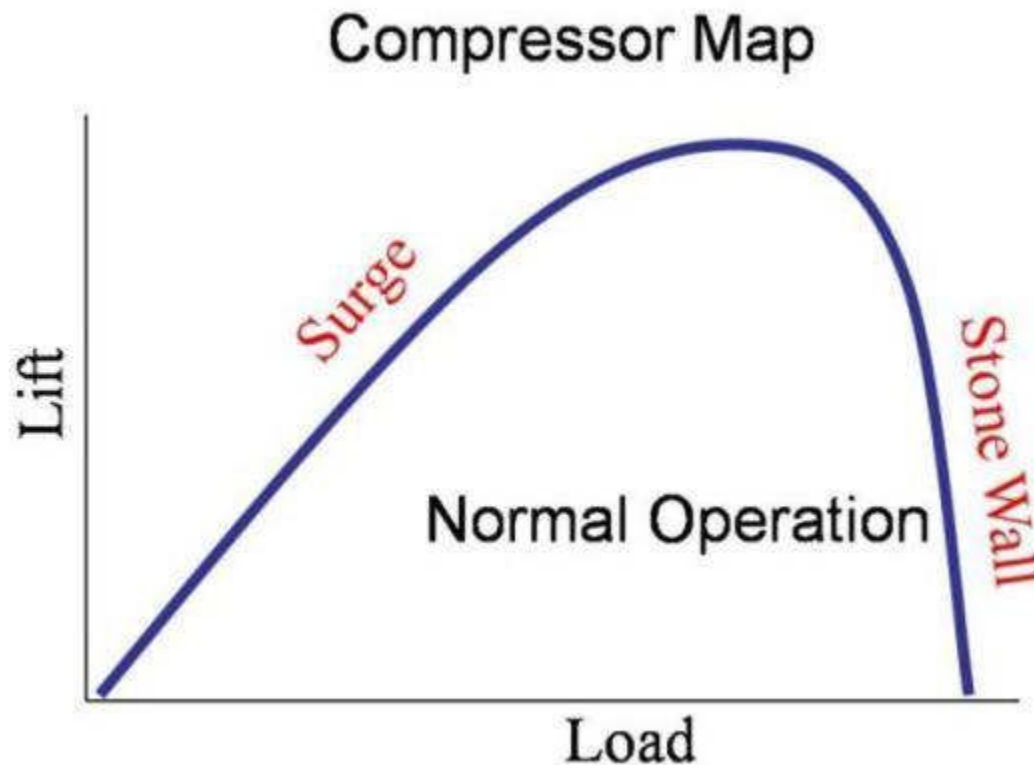


Chart-Performance of centrifugal compressor
Head output is a function of speed and inlet volume

Compressor Theory



Choke/Stonewall

Capacity of an impeller

Maximum capacity

Compressor cannot maintain required flow to maintain lift

Stall/Surge – insufficient flow result

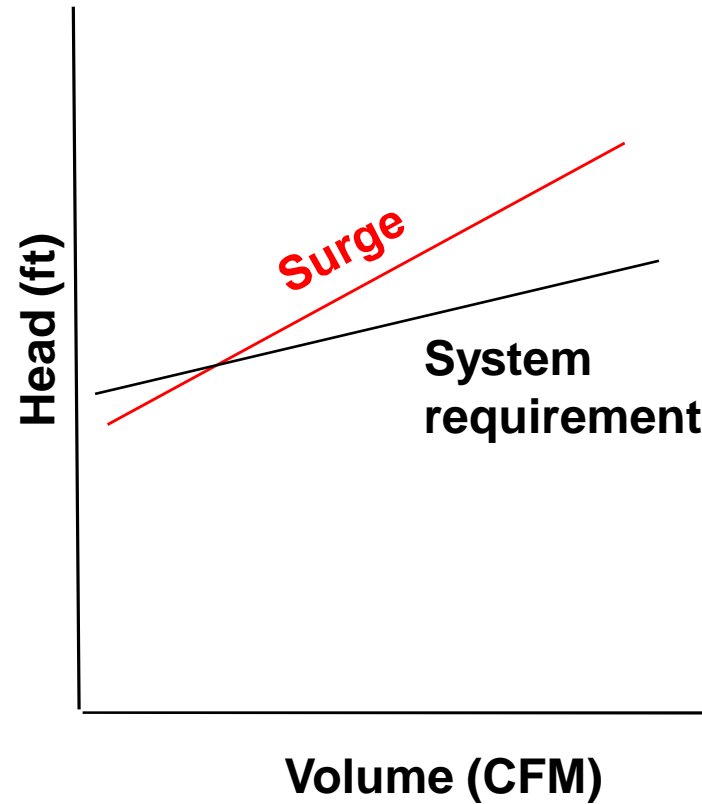
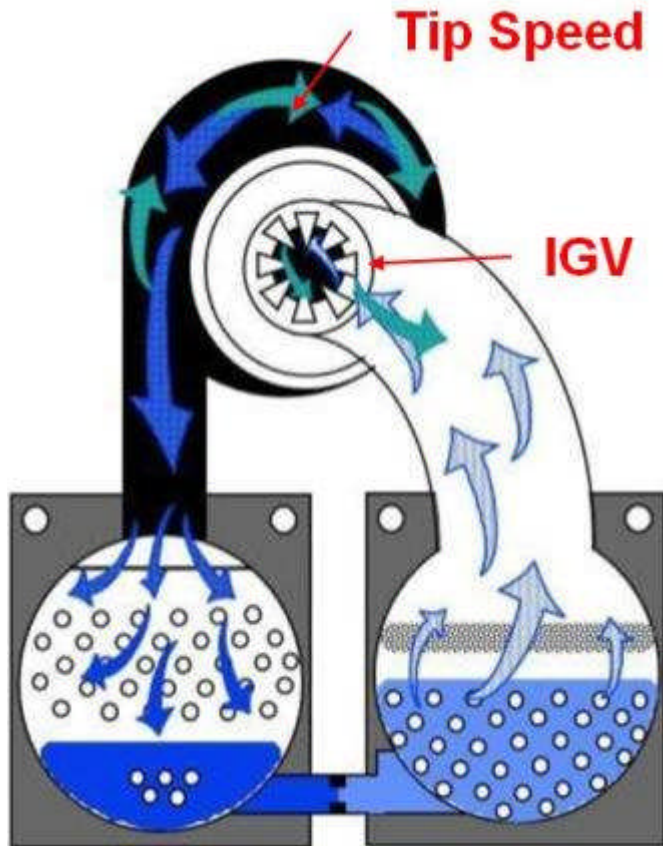
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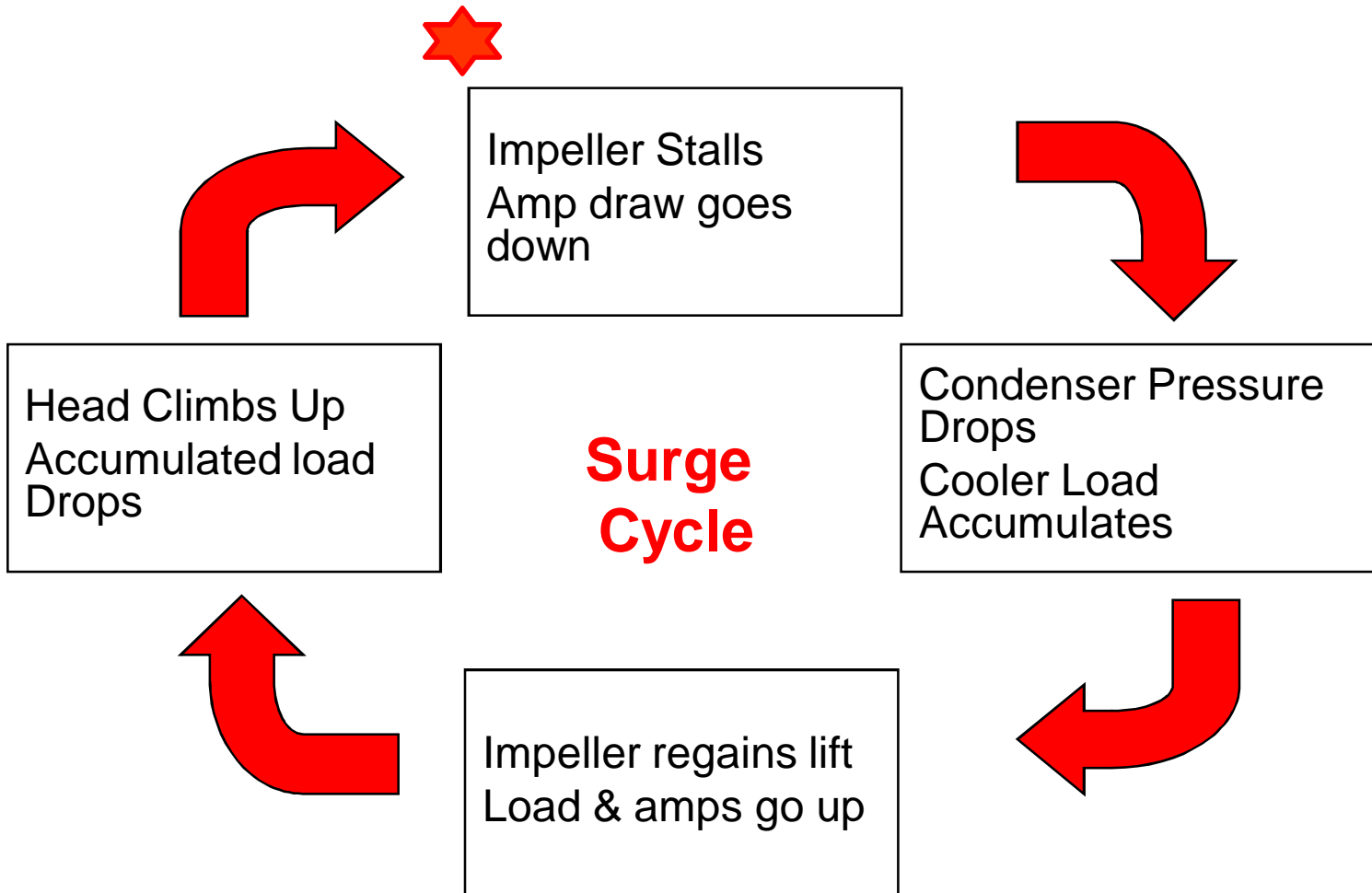
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What is Surge ?

Momentary reversal of gas flow caused by the inability of compressor to make required 'lift' for the available load



What is Surge ?

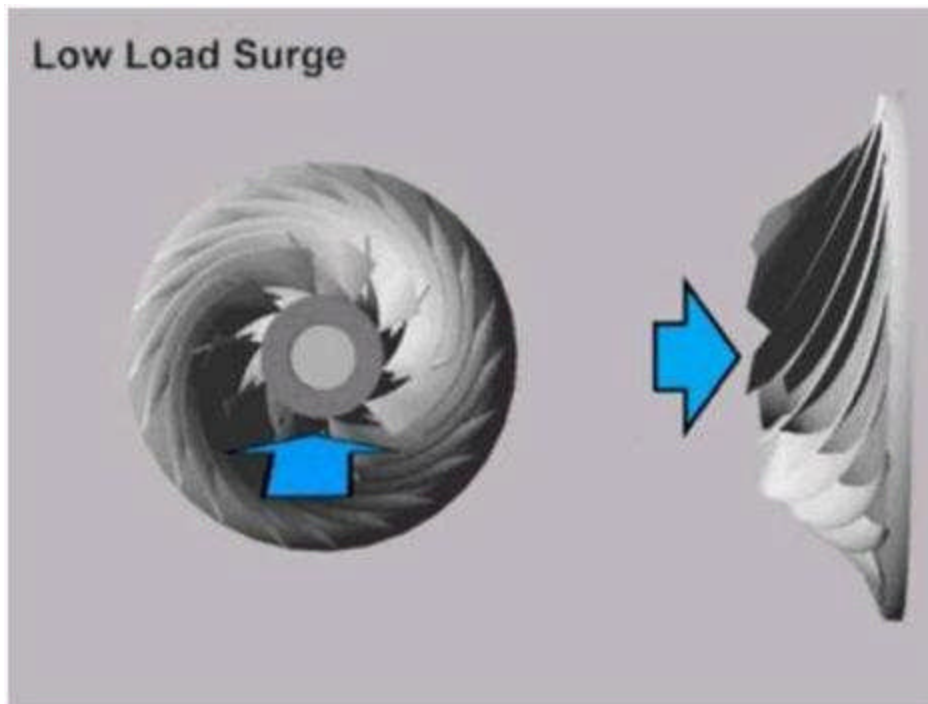


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Surge – Cooler Low Suction Press Surge



- Low Refrigerant Level
- Low Charge
- Float Valve Restriction

- Low Chilled Water Flow
- Bypass Division Plates
- Dirty/Blocked Tubes
- Air in Water Lines
- Dirty Strainer
- Pump/Valves

- Carryover
- Excessive Oil in Refrigerant
- Overcharge of Refrigerant

- Load Changes
- Hot Gas Bypass Malfunction
- Rapidly Changing Load

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Surge – Condenser High Head Press Surge

Air in Machine

High Entering Water Temperature

Low Water Flow

Bypass Division Plate

Blocked Tubes

Air in Water Lines

Dirty Strainer

Pump/Valves

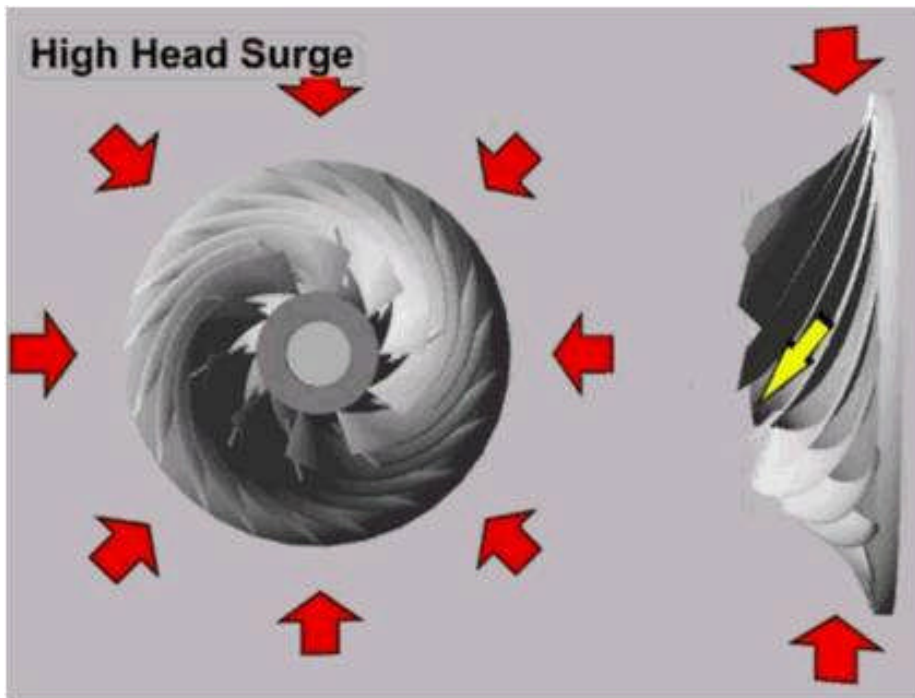
Poor Tower Operation

Fan Control Improperly Set

Bypass Water/Air

Strainer Plugged

Fan Pitch



Dirty or Scaled Tubes

Wrong Refrigerant Charge

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Surge – Compressor



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- Excessive Impeller clearance
- Failed impeller
- Wrong Impeller selection
- Low Speed - Low Voltage
- Inlet Guide Vanes Closed



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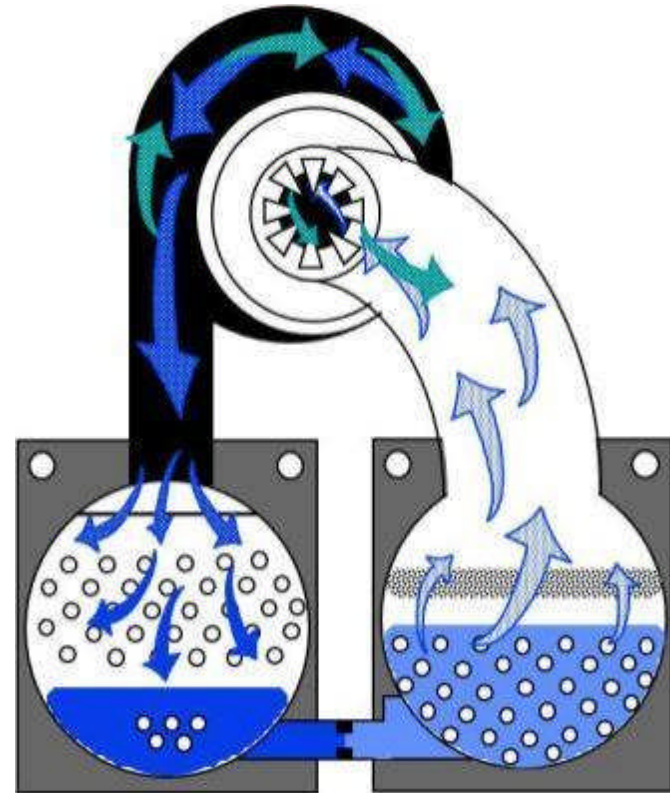
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Chiller Surge Protection

Shutdown will be initiated when > 5 surge counts have occurred within an operator-specified time

With VFD machines a surge count will increase speed by the configured % amount (VFD INCREASE STEP).

While the SURGE PROTECTION COUNTS are > 0 , a speed decrease will not be honored.



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Chiller Surge Protection

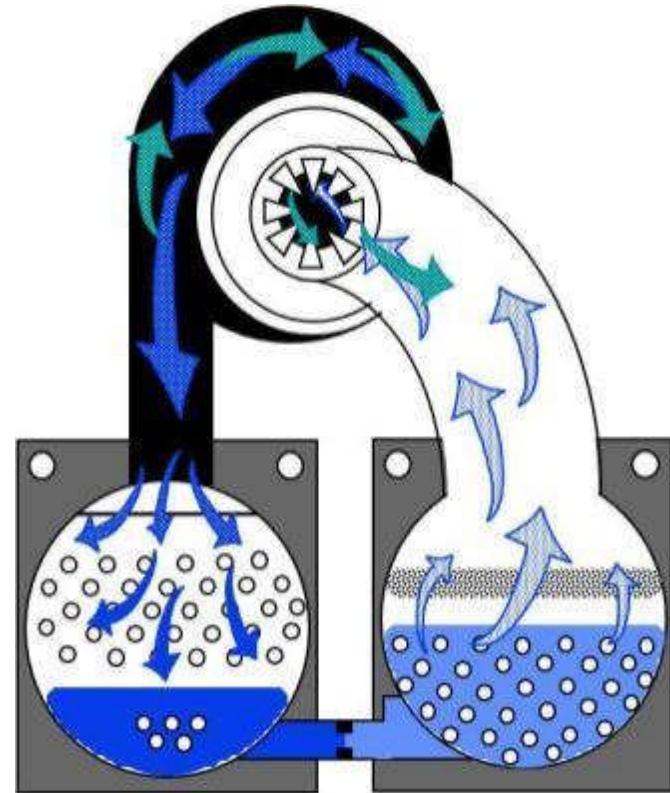


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Shutdown will be initiated when > 5 surge counts have occurred within an operator-specified time

With VFD machines a surge count will increase speed by the configured % amount (VFD INCREASE STEP).

While the SURGE PROTECTION COUNTS are > 0 , a speed decrease will not be honored.



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Maintenance



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Routine Inspection

- ✓ Check in with the customer and discuss any operational issues or problems
- ✓ Perform a visual check of the unit and listen for any unusual noises
- ✓ Record operating conditions
- ✓ Review the equipment logs made by the operators
- ✓ Perform visual inspection of auxiliary equipment, such as water pumps and tower

The greatest energy savings can be achieved with a system that operates as it was originally designed.

This requires a maintenance program that keeps the components operating at the original specifications.

Maintenance Summary

Min Requirement for Annual Maintenance

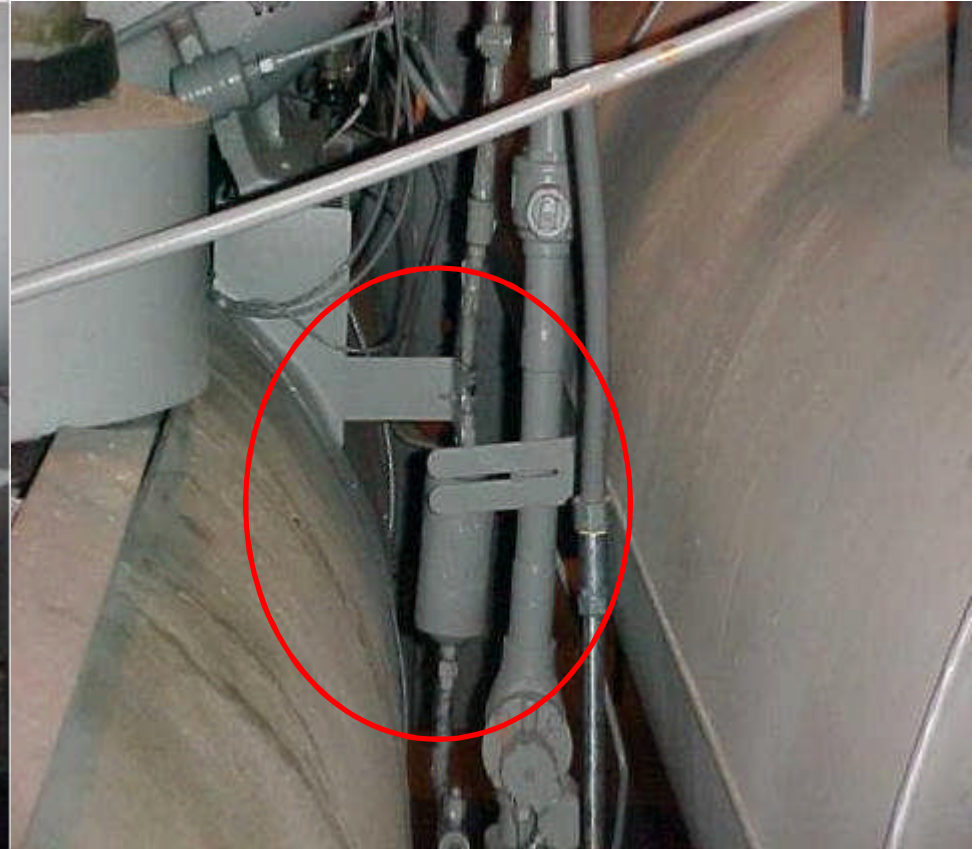
1. Replace the refrigerant filters
2. Replace the oil filters
3. Replace the refrigerant strainers when the refrigerant is transferred
4. Calibrate the transducers and check the sensors annually
5. Remove oil sample for analysis before annual service
6. Leak Test the unit for refrigerant leaks
7. Tighten all electrical connections and inspect the components
8. Inspect the tubes and clean as necessary
9. Measure Water Pressure Differentials and compare to design
10. Review operating logs, alarm history, and discuss equipment operation with the operator

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1. Replace refrigerant filters

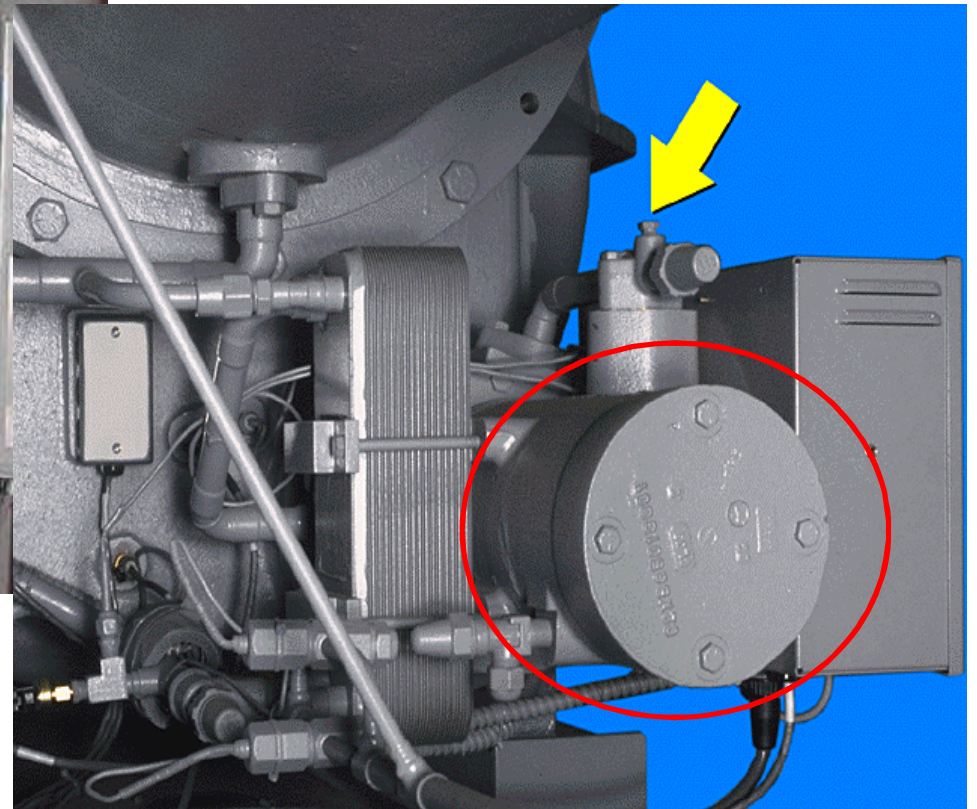
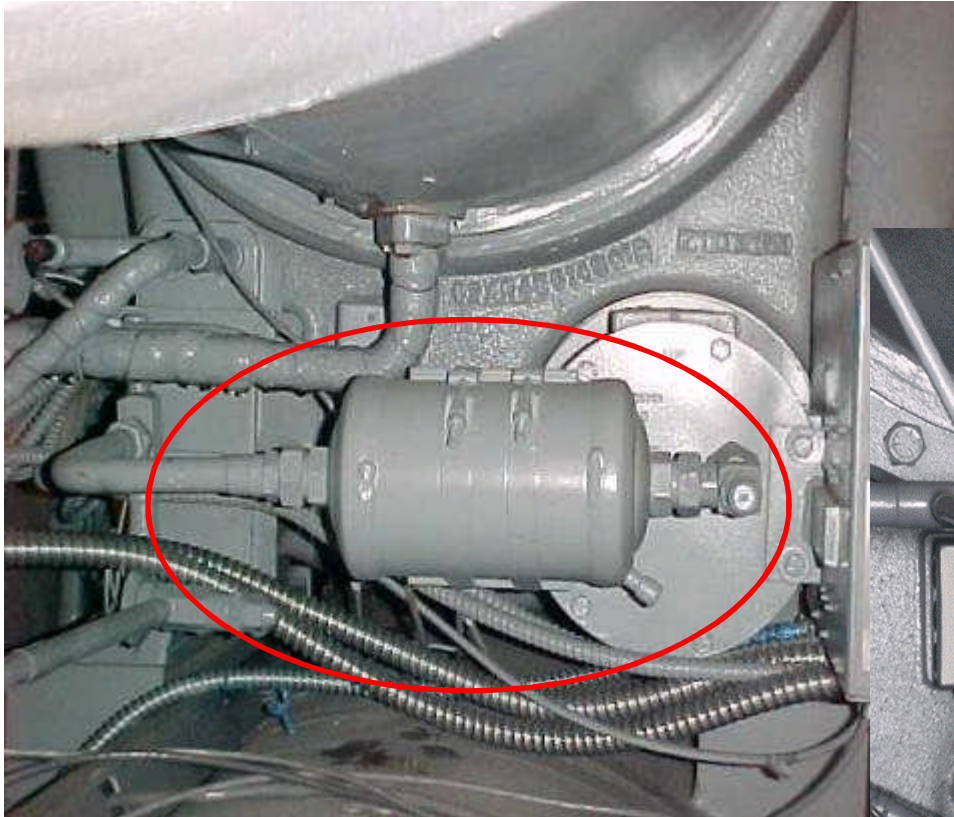


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2. Replace oil filter cartridge



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3. Replace the refrigerant strainers when the refrigerant is transferred



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4. Calibrate the transducers and check the sensors annually



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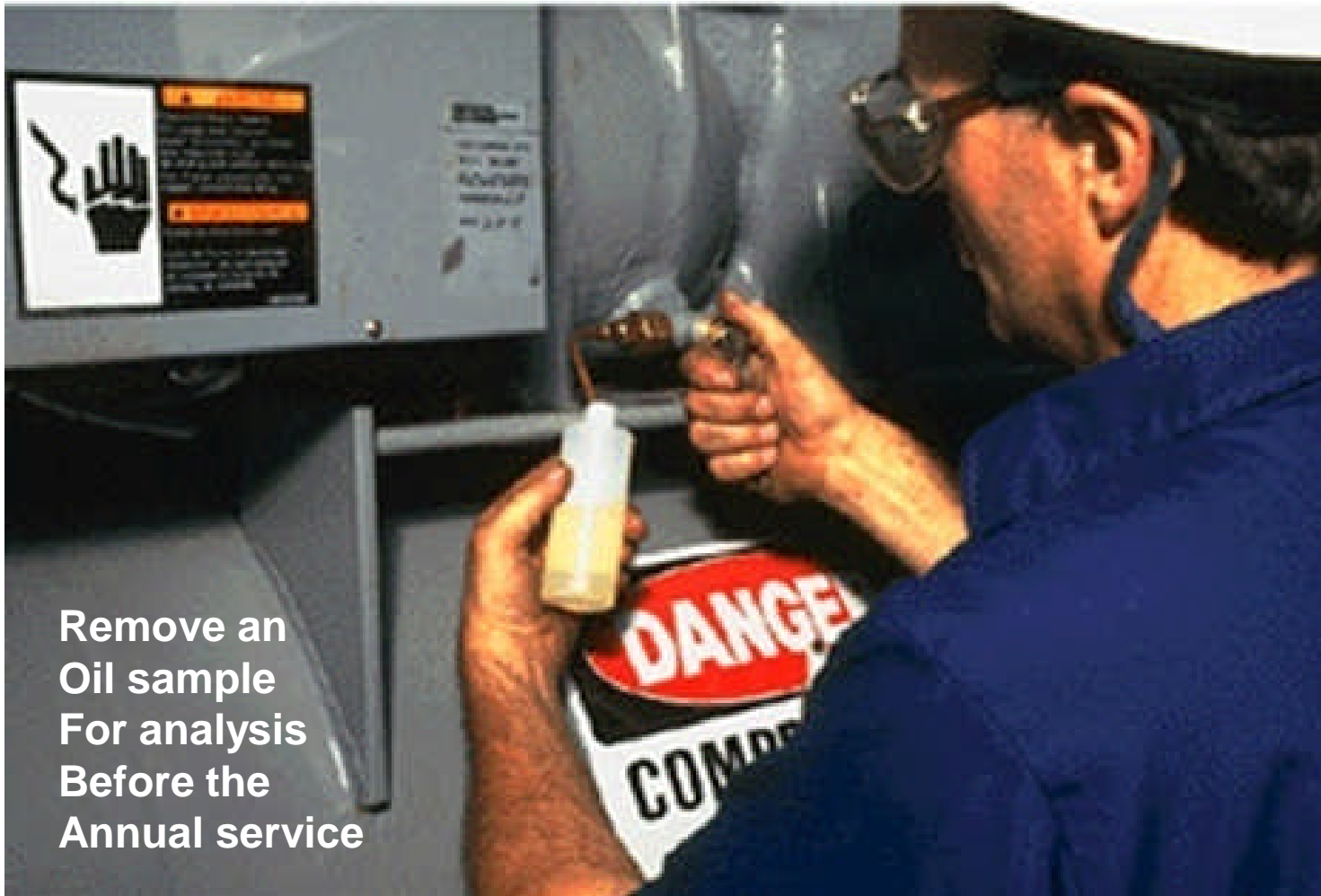


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5. Remove oil sample for analysis before annual service



Remove an
Oil sample
For analysis
Before the
Annual service

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Oil Analysis



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Test	Causes
Lubricant Type	<ul style="list-style-type: none">• Check to confirm appropriate lubricate type is in the system
Moisture	<ul style="list-style-type: none">• Weakens strength of lubricating film• Contributes to degradation of refrigerant• Contributes to creation of acid• Increases corrosiveness of acids
Acid Number	<ul style="list-style-type: none">• Slow increase in over time is normal• Large change indicates either breakdown of refrigerant or severe oxidation of oil• High acid # will contribute to corrosion in the system
Wear Metals	<ul style="list-style-type: none">• Iron, copper, chromium, tin, nickel, aluminum, lead<ul style="list-style-type: none">○ Gradual increase over time is acceptable○ Sudden increase indicates abnormal wear• Zinc/Phosphorus are anti wear additives that will decrease gradually over time

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Oil Analysis (continue)

Test Parameters	Causes
Chloride/Fluoride	<ul style="list-style-type: none">• High Levels results from breakdown of refrigerant• Good indicator of refrigerant health
Ion Activity	<ul style="list-style-type: none">• High ion activity is caused by any one or combination of the high levels of wear metals, high acid #, high chloride/fluoride, high moisture• Gradual increase over time
Viscosity	<ul style="list-style-type: none">• Dissolved refrigerant, oxidation of lubricant, excessive contamination changes viscosity• Not a common problem in HVAC
Mixed Oil Percentage	<ul style="list-style-type: none">• Identify contamination from other lubricants• Verify completion of a conversion from mineral to synthetic oil

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Sample Oil Analysis Report



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Carrier Job No. : 059A11043				Report Number : RR078280-001			
Job Name : La Tour				Date Sampled : 8/30/2012			
CCS Office : CCS Dallas/DFW Ctrls(59/50)				Sampled By : B Boone			
Manufacturer : Carrier				Contact Person : Chris Higgins			
Unit Model : 19XR4647353KDH64				Date Received : 9/5/2012			
Serial Number : 0407Q73656				Date Analyzed : 9/6/2012			
Equipment ID : 0407Q73656				Reported By : Gintare Scott			
Machine Hours : 24614							
				Previous Samples			
	Units	Limits	Current Sample	11/8/2010	2/9/2009	2/7/2008	
Water	ppm	< 300	126	33	43	11	
Acid Number	mg KOH/g	< 0.5	0.076	0.027	0.058	0.034	
Chloride	ppm	< 20	<3	<3	<3	<3	
Fluoride	ppm	< 20	<3	<3	<3	<3	
Ion Activity	mmhos	< 200	27	38	43	23	
Aluminum	ppm	< 15	<1	<1	<1	<1	
Copper	ppm	< 400	<1	<1	<1	<1	
Chromium	ppm	< 15	<1	1	<1	<1	
Iron	ppm	< 25	<1	1	<1	<1	
Nickel	ppm	< 15	1	2	<1	<1	
Lead	ppm	< 15	<1	<1	<1	<1	
Tin	ppm	< 15	1	3	1	<1	
Zinc	ppm		3	4	4	<1	
Phosphorus	ppm		<1	13	3	<1	
Oil Type			POE	POE	POE	POE	

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6. Leak Test the unit for refrigerant leaks



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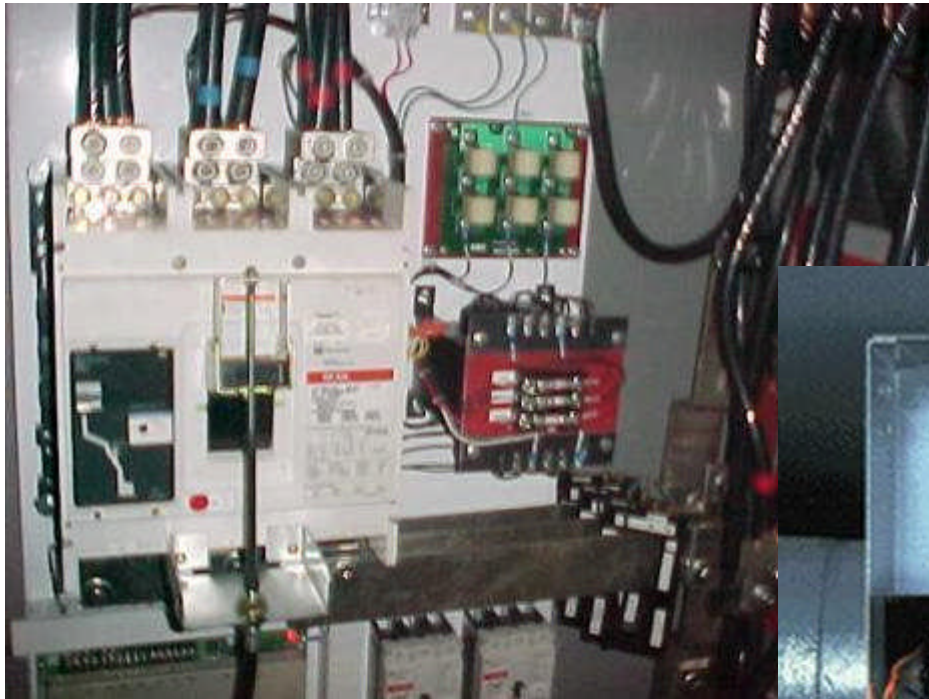


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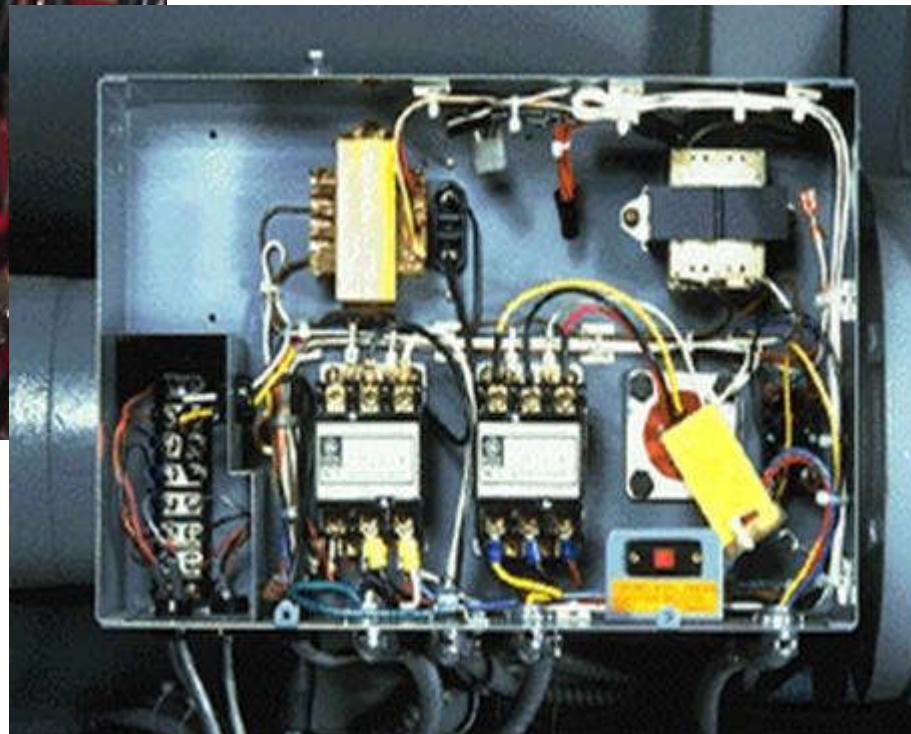


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7. Tighten all electrical connections and inspect the components



Clean enclosure and components
Of dirt and debris



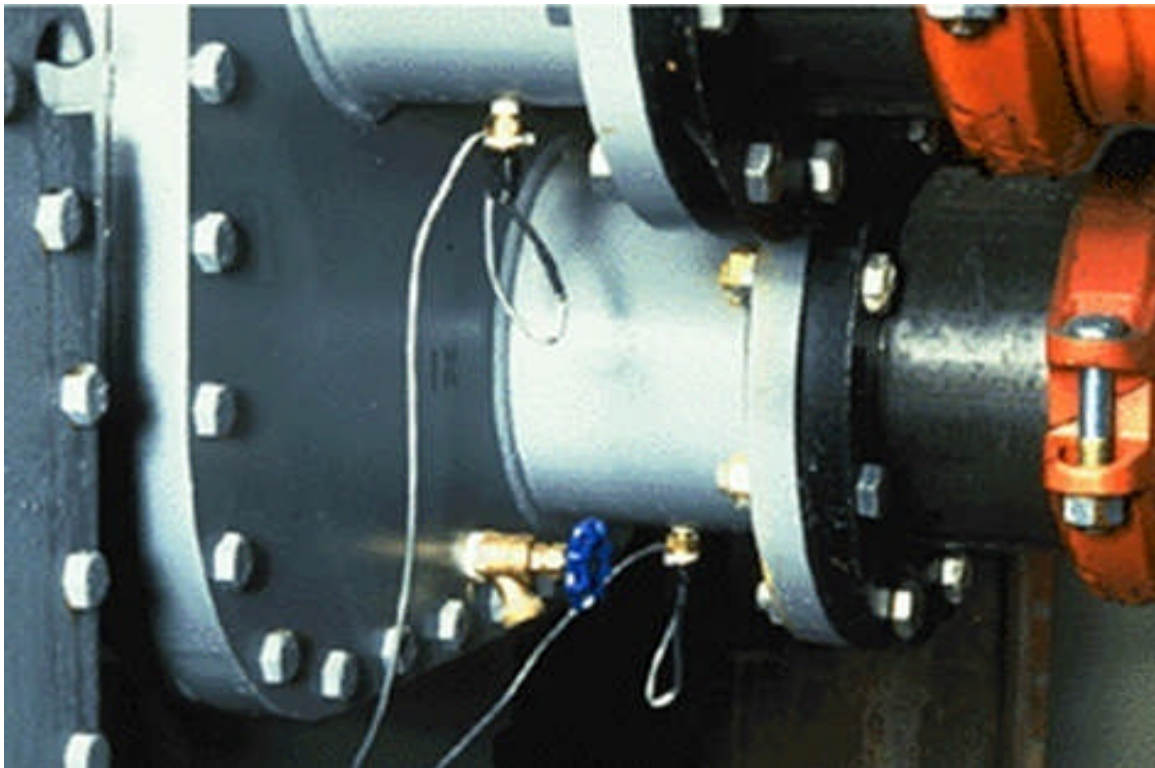
Check the condition of
And
Tighten the Electrical Connections
In the Starter and Control Panels

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8. Remove the Water Box Covers and Inspect Tubes Cleaning as Necessary



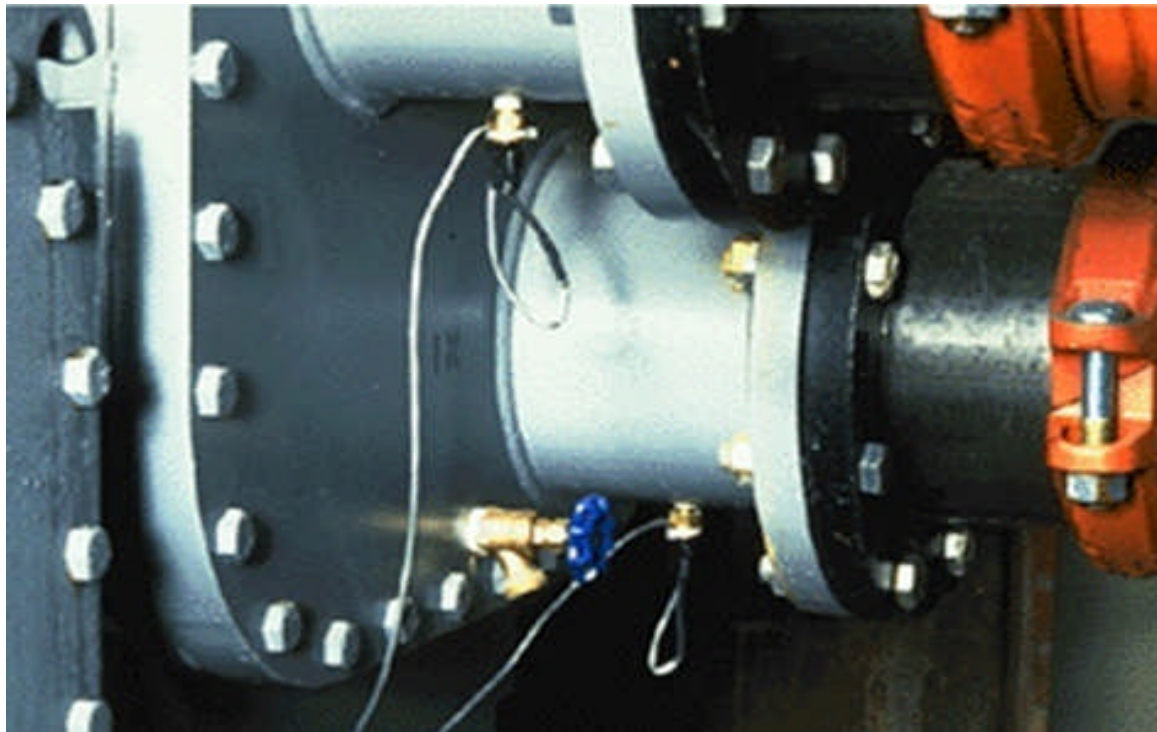
Water Circuits exposed To the atmosphere should Be inspected annually. Closed circuit water loops Can be inspected at Longer intervals.

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9. Measure Water Pressure Differentials and compare to design



- If not at design:
1. Check Strainers
 2. Valve position
 3. Piping changes

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10. Review operating logs, alarm history, and discuss equipment operation with the operator



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Other suggested task: Starter Check

Wye Delta Design- check the contactors, tighten electrical connections, inspect the transition resistors, and check the motor resistance with a meg-ohm meter.

Solid State- check the resistance of the SCR's that is provided by the manufacturer, inspect the bypass contactors, tighten electrical connections, and check the motor resistance with a meg-ohm meter with the motor leads disconnected from the starter.

Variable Speed Drives- check the resistance of the rectifier/filter/inverter with comparison to the manufacturer limits, replace cooling fans as required, verify the accuracy of the current/voltage/frequency displays, and check the motor resistance with a meg-ohm meter with the motor leads disconnected from the starter

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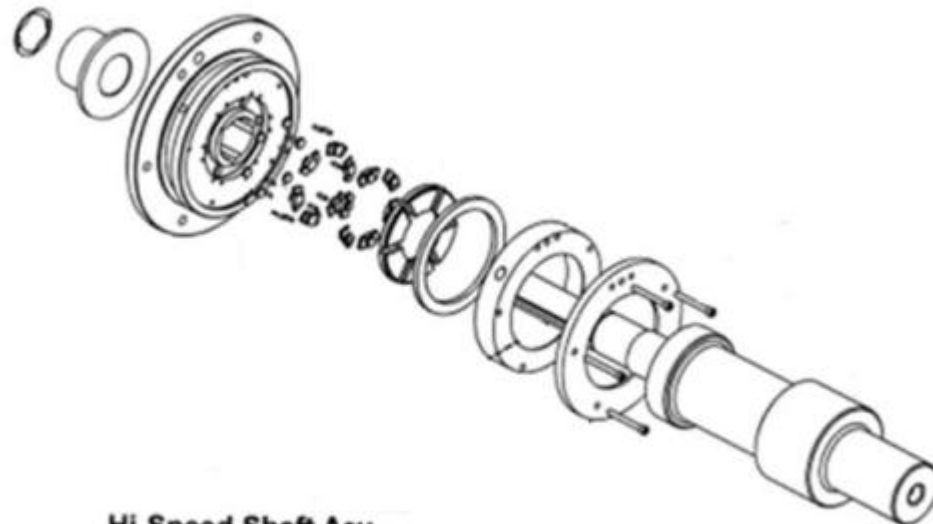


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Other suggested task: Vibration Analysis

A compressor with rolling element bearing design will require vibration trending to determine bearing wear.

Oil analysis will provide the condition of the oil, but will not indicate bearing wear as it would with a babbitt surfaced bearing with an increased tin level.



Hi-Speed Shaft Asy
Compressors Without Roller Element Bearings

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Good Service Practice



- ✓ Always evacuate any area opened for service to prevent non-condensables from entering the system
- ✓ Leak test the area after completion of the work
- ✓ Turn in oil sample as quickly as possible to prevent potential contamination
- ✓ Clean up your work area and complete all paperwork

19XRV SERVICE UPDATES

Chiller Efficiencies Maintenance



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Chiller efficiency

The following factors can reduce chiller efficiencies

1. Air/Non-condensables
2. Scaled or Dirty Condenser Tubes
3. Low Condenser water flow
4. Refrigerant (contaminated, too much, too low)
5. Excessive chilled water flow
6. Dirty chilled water tubes

19XRV SERVICE UPDATES



Air in the machine

ΔP across condenser is at design, and ΔT across condenser fairly close to design

Approach is above design

Gauge pressure(converted to temperature) and condensing liquid temperature is greater than 1-2°F

This means that there is non-condensables in the machine

Recommendations

Remove Air

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Fouled condenser tubes

ΔP across condenser is near design, and ΔT across condenser is less than design

Approach is above design

There is no non condensables in the heat exchanger as gauge pressure (converted to temperature) and condensing liquid temperature is within 1-2°F

Heat transfer surface area is reduced, condensing temperature increase which increase the lift

Recommendations

Clean tubes

Ensure water treatment is corrected

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Low condenser water flow

ΔP across condenser is less than design, and ΔT across condenser greater than design

Approach is slightly above design

Gauge pressure(converted to temperature) and condensing liquid temperature is within 1-2°F

Latent heat cannot be removed if flow is low

The condensing temperature will increase which will increase lift

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Low condenser water flow (continue)

Causes

- Plugged strainers at pump or tower

- Closed valves

- Pumps are performing/sized improperly

- Air in condenser water system

- Plugged tubes

Recommendations

- Clean strainers

- Open valves

- Correct Pumping station

- Bleed air from condenser water circuit

- Clean tubes

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Low Chilled water flow

ΔP across condenser is less than design, and ΔT across condenser greater than design

Approach is above design

Causes

Plugged strainers

Closed valves

Pumps not performing/sized properly

Plugged Tubes

Air in Water

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Low Chilled water flow (continue)

Recommendations

Clean strainers

Open valves to correct ΔP

Correct pumping stations

Clean tubes

Bleed air from chilled water system

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Refrigerant charge

Low refrigerant charge

Compressor will compensate by lowering cooler pressure

Cooler refrigerant temperature will drop

Lift the compressor has to make will increase

High refrigerant charge/contaminated refrigerant

Cooler pressure will lower

Risk of flooding the compressor

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Low Refrigerant charge at cooler

ΔP across condenser is at design, and ΔT across condenser is less than design

Approach is above design

Low motor amps at full capacity

Causes

- Leak/lost of charge

- Float valve not working

- Refrigerant stacking in condenser

- Too much oil

Recommendations

- Repair leaks

- Add refrigerant

- Check float valve

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Condenser water bypassing condenser tubes

ΔP across condenser is less than design, and ΔT across condenser is less than design

Approach is above design

Causes

- Division plate gasket ruptured

- Broken division plate

Recommendations

- Reinstall division plate gasket

- Repair/replace broken division plate

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Chilled water bypassing chilled water tubes

ΔP across condenser is less than design, and ΔT across condenser is less than design

Approach is above design

Causes

- Division plate gasket ruptured

- Broken division plate

Recommendations

- Reinstall division plate gasket

- Repair/replace broken division plate